

REPORT NUMBER: 3083303SAT - 004 REV1

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> EVALUATION CENTER Intertek Testing Services NA, Inc. 16015 Shady Falls Road Elmendorf, TX 78112

EPORT

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RENDERED TO

Emmedue S.P.A. Via Toniolo, 39/b Z.I. Bellocchi 61032 Fano (PU), Italy

PRODUCT EVALUATED: 4' x 8' and 4' x 12' Single Panel PSM80 and PSM150 Wall Systems EVALUATION PROPERTY: ICC – AC 15, Section 4.2.2.6, ASTM E 72 - 05, Section 11 (Floor/Roof Flexural Load)

Report of Testing 4' x 8' and 4' x 12' Single Polystyrene PSM80 and PSM150 panels for compliance with the applicable requirements of the following criteria: *ICC – AC 15, Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems, under the general guidelines of ASTM E* 72 - 05, Standard Test Methods of Conducting Strength Tests of *Panels for Building Construction*

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2 Introduction

Intertek Testing Services NA, Inc. (Intertek) has conducted testing for Emmedue S.P.A on 4' x 8' and 4' x 12' Single Polystyrene PSM80 and PSM150 structural wall panels. The test method consisted of the transverse-flexural load under third-point loading. Emmedue wall systems are based on a series of foam polystyrene panels and electro-welded steel wire meshes, whose shapes have been specially designed to apply structural plaster during panel installation (Ref, 1, p. 3). These systems are capable of multiple applications, such as quick installation and high thermal and sound capabilities (Ref 1, p. 3). The purpose of these tests is to evaluate flexural load structural applications according to Section 4.2.2.6 of ICC – AC 15, under the general guidelines of ASTM E 72 - 05, Conducting Strength Tests of Panels for Building Construction. The results of each test are presented in tabular and graphical form. In total, 12 specimens were tested under the above loading configuration to measure the deflection and failure characteristics of each of the wall systems. This evaluation began November 19, 2007 and was completed November 29, 2007.

NOTE: This report is only for the transverse floor/roof flexural tests performed. Refer to report numbers **3083303SAT - 001, - 002, - 003, - 005, - 006, - 007, and - 008** (designated **REV1, except 008**) for the rest of the testing completed for this project.

3 Test Samples

3.1. SAMPLE SELECTION

Samples were randomly selected on July 1, 2007 by Intertek representative Matt Lansdowne, EIT, at the Emmedue S.P.A manufacturing facility, located at Via Toniolo 39/b, Z.I. Bellocchi, 61032 Fano (PU), Italy. Samples were received at Intertek – San Antonio on August 28, 2007.

The subject test specimens are traceable samples selected from the manufacturer's facility. Intertek selected the specimens and has verified the composition, manufacturing techniques and quality assurance procedures.

Refer to the Pre-Test Inspection Report, dated July 1 - 2, 2007, located in the Appendix.

3.2. SAMPLE AND ASSEMBLY DESCRIPTION

The Emmedue Single Panel PSM80 and PSM150 consist of a foam polystyrene core reinforced with a galvanized steel wire mesh connected on both sides of the foam using corrugated steel bars. The steel bars and mesh are electro-welded together for strength. There are approximately 82 connectors per square meter of foam surface. Below is a list of specifications of the PSM80 and PSM150 panels (Ref 1, p. 7). The numbers below were converted from metric to inch-pounds from the Emmedue Operator's Handbook.

Galvanized Steel Wire Mesh

- 1) Longitudinal wires with diameter of 0.121 inches spaced every 2.56 inches
- 2) Transversal wires with diameter of 0.099 inches spaced every 2.56 inches



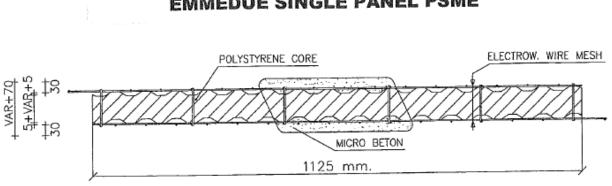


Figure 1: Emmedue Single Panel PSM80 and PSM150 Details (Ref. 1, p.7)

15 Kg/m³ (0.936 lb/ft³) Polystyrene Slab Density: Polystyrene Slab Thickness: 4" (PSM80) and 6" (PSM150)

The Emmedue building system comprises of different wall, floor, and roof arrangements that are finished on-site using sprayed mortar and concrete. Although different techniques exist for spray mortar, the mortar mix used for this project consisted of Portland[®] Cement, sand, and water. The client recommends an average quantity of plaster (or mortar) of about 1 inch sprayed per side. The recommended concrete thickness for floor/roof walls is approximately between 2" and 2 1/2". These panels are generally used for buildings of no more than 4 stories high, in seismic areas, for floor slabs and covering slabs whose spans are 4 m (13.12 ft) at maximum (Ref. 1, p. 7).

For these tests, a mortar mix design was provided in order to meet the required wall structural plaster specifications. The mortar mixing ratio (by weight) was provided as followed:

Portland [®] Cement:	100 lbs
Sand:	280 lbs
Water:	5.0 gallons

The above numbers were provided by the client during sample construction. As indicated by the Emmedue Operator's Handbook (Ref. 1, p 27), the quantity of water should vary as humidity and temperature changes are observed. Accordingly, modifications to the mixing ratio were made as indicated by the weather conditions during mortar spraying. In all cases, the minimum compressive mortar strength (f'c) was 2500 psi at 28 days curing time. These results were verified by performing mortar cylinder core tests at 7 and 28 days as per ACI 506.2, for each batch made. Additional mortar cylinder core tests were also performed within 48 hours of the completion of each set of three full-scale tests, as per AC 15, Section 4.2.2.6.

From the mortar cylinder core testing results obtained, it was found that no mortar core was lower than 2500 psi at 28 days. Refer to report number 3083303SAT - 008 for a complete listing of all mortar core tests performed.

Both the PSM80 and PSM150 floor/roof panels were constructed with a concrete top and a sprayed mortar bottom. The nominal concrete thickness was between 2 inches and 2 ½ inches.



EMMEDUE SINGLE PANEL PSME

The nominal mortar thickness was approximately 1 inch. The concrete specifications were as followed:

Compressive Strength (f'c):3500 psi at 28 daysConcrete slump:5 inches (using an Abram's slump cone)Aggregate size:Nominal 3/8" pea gravel

The concrete was ordered through a local supplier. The mix design was also provided by the concrete supplier. A detailed copy of the concrete mix design used is located in the Appendix.



4 Testing and Evaluation Methods

4.1. Construction of Floor/Roof Assemblies

Twelve transverse floor/roof flexural samples were tested and all were constructed in the same manner. The floor/roof panel test matrix was as followed:

Panel Type	Size	No. of Tests
PSM80	4' x 8'	3
PSM80	4' x 12'	3
PSM150	4' x 8'	3
PSM150	4' x 12'	3

Construction of the 4' x 8' and 4' x 12' samples consisted the following:

- 1) Single Panel PSM80 and PSM150
- 2) 1/8" Rebar tie wire
- 3) 1x10 #1 yellow pine lumber cut down to 7 $\frac{1}{2}$ wide for PSM80 panels
- 4) 1x10 #1 yellow pine lumber cut down to 9 ½" wide for PSM150 panels
- 5) #8 x 2" wood deck screws
- 6) Mortar mixture (Portland[®] Cement, sand, and water)

All of the samples had to be constructed at the Intertek-San Antonio facility. Panel assembly first consisted of constructing a wooden frame around the perimeter of the PSM80 panel using #8 x 2" wood deck screws and 1x10 #1 yellow pine lumber joists cut down to 7 $\frac{1}{2}$ " wide. The difference in thickness accounts for the two different thicknesses of mortar and concrete. The PSM150 panel frames were constructed in the same manner, however, the 1x10 #1 yellow pine was cut 9 $\frac{1}{2}$ " wide. The perimeter frame served two purposes: 1) as a support to assure that each wall was even and plumb before mortar spraying, and 2) as a guide for applied proper mortar thickness. For the 8 foot samples, the 1/8" rebar tire wire was installed 32" from the top and bottom around the panel and frame in order to hold the two pieces together. For the 12 foot samples, the rebar tie wire was installed at 48" from top and bottom. Refer to Figure 2 for more details.





Figure 2: Finished wood frames with 4' x 12' panels ready for spray mortar application

The samples were then sprayed with a mortar mixture of sand, water, and Portland[®] Cement on one side using a plaster sprayer provided by the client. Mortar specifications included sand particles with less than 0.20" size and a slump of 2", at the appropriate ratio (refer to Section 3.2, Sample and Assembly Description, for mixing ratio). The three ingredients were mixed using a concrete mixer. A compressor capable of adjustment was used in order to assure the client recommended 90 psi application pressure. Two layers of sprayed mortar were applied to one side until the desired mortar thickness of 1" (+/- $\frac{1}{4}$ ") was achieved. The samples were then smoothed out as much as possible using mortar trowels or any other straight smoothing device. Refer to Figures 3 and 4 for details.



Figures 3 and 4: Mortar mixing and spraying application on 4' x 12' assemblies, respectively



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The sprayed mortar samples were allowed to cure for approximately 7 days. Once cured, the samples were flipped over and repositioned horizontally on the floor. This was done in order to prepare the samples for concrete pouring. All floor/roof flexural samples were poured on 10/3/07. The concrete was poured from the truck into wheel barrels which were then carted to the appropriate samples. The concrete was gravity poured and settled using a concrete vibrator. Once poured, the tops of the samples were smoothed out using a trowel (or some other type of smoothing device). The samples were then wetted down for a period of 24 hours in order to avoid accelerated curing of the concrete (which can lead to surface cracks). Refer to Figures 5 through 7 for details.



Figures 5 and 6: Floor/roof panels prepared for concrete pouring



Figure 7: Finished floor/roof panels with concrete wetted down

The samples were allowed to cure for at least 28 days prior to testing. All 12 floor/roof flexural sample configurations (4' x 8' and 4' x 12') tested were equal in construction techniques.



4.2. ICC-AC 15 and ASTM E 72 - 05 Testing Procedures

Transverse-Flexural Load Procedure (Third Point Loading)

The test rig consisted of a steel rigid A-frame, specimen supports, steel support rollers and bearings, and a hydraulic cylinder. The setup procedure consisted of positioning concrete specimen supports at the given span length (L) for each specimen. These concrete supports were made of solid 7 $\frac{1}{2}$ " x 7 $\frac{1}{2}$ " x 15 $\frac{1}{2}$ " concrete blocks. A total of three concrete blocks were positioned at each end of the support span length. Once the blocks were laid out at the proper distance, two 1" diameter x 50" long steel rollers and two 3" wide x 50" long x $\frac{1}{4}$ " thick steel bearing plates were positioned at the proper support span length (L) on top of each row of blocks. For the 8 foot samples, the support span was 93 inches and for the 12 foot samples, the support span was 141 inches.

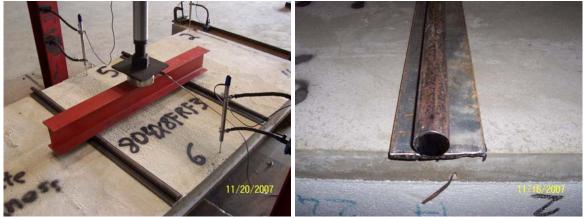
Once the roller end bearings were positioned, the samples were carried and lifted in place using a forklift and lifting straps. Each sample was then lowered in place on top of the roller bearings. Adjustments were made accordingly to the sample and roller bearings in order to obtain the appropriate support span. <u>All floor/roof flexural samples were tested with the concrete side up (loaded side).</u> Refer to Figures 8 and 9 for details.



Figures 8 and 9: Floor/roof flexural test setup (4' x 8') and 3" wide roller end bearing

After adjusting the sample, the loading bearings were positioned on top of the sample. The purpose of these bearings was to evenly distribute the load through two points under third-point loading conditions. The bearings were positioned 31 inches apart for the 8 foot samples and 47 inches for the 12 foot samples. These two loading bearings were of the same specifications and materials as the end reaction bearings. A loading I-beam was then positioned perpendicular to the loading bearings exactly at the midpoint of the wall (24 inches in width). A calibrated load cell was then installed on top of the loading beam. The head of the hydraulic cylinder was then lowered until it touched the top of the load cell. This assured proper alignment of all the components, as well as holding the sample in place. Refer to Figures 10 and 11 for details.





Figures 10 and 11: Third-Point loading setup (top view) and top loading bearing location

The deflection measurement gauges consisted of six spring loaded 4" low voltage displacement transducers capable of 0.001 inch resolution. Transducer data is logged and stored via a data acquisition unit. The transducers are supported using mechanical adjustable arms with a magnetic base that connect to a rigid steel bar which are attached to two cinder blocks. The blocks rest on the concrete floor of the laboratory.

All testing was performed according to Section 4.2.2.6 of ICC – AC 15, under the general guidelines of ASTM E 72 - 05, Section 11 loading procedure. Once the specimen was properly installed on the frame, two linear transducers (with 0.001 inch resolution) were placed centrally along the lateral dimension of the specimen at opposite sides of the specimen along the short dimension (width) no more than 2" from the specimen edge. Four transducers were placed on each corner of the specimen at 1 $\frac{1}{2}$ " in from the side and at 1 $\frac{1}{2}$ " in from the end to measure the uplift as the specimen is loaded.

A pre-load (not to exceed 10% of the ultimate load) was applied to the specimen. With the preload applied to the specimen, an initial reading is made. All set load readings are taken at this pre-load reading, which is labeled as the "zero" mark. Once this measurement is made, the load is increased slightly which in turn applies an initial load to the specimen. The load is applied for 5 minutes during which time deflection measurements are made as a function of time (as soon as it is practical after initial loading and at the end of the 5 minute period). After the 5 minute period, the load is decreased to the "zero" load (a.k.a. the predetermined pre-load) for 5 minutes during which time deflection measurements are made as a function of time (as soon as it is practical after initial un-loading, and at the end of the 5 minute period). The process is repeated in increments of "n" of initial load (n = 2, 3, 4,...) until a predetermined number of data points is obtain to effectively plot a load-deflection curve. Once the appropriate number of points is reached, the instruments are removed and the test specimen is loaded to failure. Refer to Figure 12 for details.





Figure 12: Floor/roof flex test setup for 4' x 12' samples (overall view)

Refer to Appendix C for floor/roof flexural test photos.

4.2.1. ICC – AC 15 and ASTM E 72 - 05 Notes

These tests were performed in accordance to ICC- AC 15 and under the general guidelines of ASTM E72 – 05. As per ICC – AC 15, six specimens were tested, using two different configurations and/or heights. The tested specimens consisted of equal widths (4 feet), <u>different</u> thicknesses (7 $\frac{1}{2}$ " and 9 $\frac{1}{2}$ ", as per PSM80 and PSM150 panel variations, respectively), and two <u>different</u> length configurations (8 feet and 12 feet).

According to AC 15, Section 4.2.2.6, three mortar cylinder cores shall be tested within 48 hours of the completion of each set of full-scale tests. This procedure was performed for each set of constructed samples, in addition to 7 and 28 day mortar cores for each batch of mortar mixed. For example, if a set of samples required two applications of sprayed mortar on one side, then six mortar cylinder cores were made for each batch of sprayed mortar (tested at 7 and 28 days for each batch). Accordingly, since these specimens also contained <u>concrete</u>, three concrete cylinder cores were also tested within the 48 hour window (at the same time as the mortar cores). Concrete cylinder cores were tested under the general guidelines of *ASTM C 39*, *Compressive Strength of Cylindrical Concrete Specimens*.

The mortar cores were made under the general guidelines of ACI 506.2 - 95, Specification for Shotcrete. Under the ACI 506.2 code, Section 1.6.1.1, the preparation of the shotcrete mortar cylinder core panels was to be made according to $ASTM \ C \ 1140$, Preparing and Testing Specimens from Shotcrete Test Panels. According to ASTM C 1140, Section 5, "...the forms for making shotcrete mortar cores shall be made of wood or steel construction and sufficiently rigid to prevent dislodging of the shotcrete through vibration or deformation." The forms were constructed of 1x6 #1 yellow pine lumber, 2x4 #2 yellow pine lumber, $\frac{3}{4}$ " plywood, and #8 x 1 $\frac{1}{2}$ " wood deck screws. The interior dimensions of the forms constructed were **24**" wide x 24" long x 3 $\frac{1}{2}$ " deep, as indicated in Section 5 of ASTM C 1140. One form was constructed for



each time a new batch of mortar was made. From each form, a total of approximately 25 cores could be made at one time. Refer to Figure 13 for details.



Figure 13: Wooden form for mortar core sampling

Once the wooden form was made, the mortar was sprayed into the form until it covered the entire $3\frac{1}{2}$ depth. The mortar was allowed to settle naturally with <u>no</u> help of any mechanical means (concrete vibrator, mixing rod, etc.). The top of the form was then smoothed out with a trowel (or any other suitable straight smoothing device) and was then moved indoors and allowed to cure for a <u>minimum of 24 hours</u>. Each sprayed form was properly labeled and sealed using plastic sheathing and shrink wrap to maintain the proper moisture. Refer to Figures 14 through 19 for details.



Figures 14 and 15: Application of sprayed mortar into wooden forms





Figures 16 and 17: Smoothing of mortar in wooden form



Figures 18 and 19: Mortar form labeling and sealing with plastic sheathing

After a minimum curing time of 24 hours, the forms were transported to an outside core testing facility and cored for the number of samples indicated. Coring was made using a specialized coring drill with a diamond bit. Once the samples were cored, they were properly labeled, measured, weighed, sulfur capped, and stored in a 100% humidity moisture room until tested.

The concrete cylinders were prepared on site by a qualified field technician from an outside concrete laboratory. Slump and temperature measurements were taken from the concrete as it was delivered by the supplier. $4^{"} \times 8^{"}$ cylinders were made on site for each concrete pour, tested at 7 and 28 days for quality assurance. The standards involved in testing the concrete cylinders include (but are not limited to) *ASTM C 31, C 192, and C 617*.

Refer to Figures 20 through 27 for more details.





Figure 20: Drilling of mortar cores



Figure 21: Mortar cores after drilling





Figures 22 and 23: Labeling, weighing, and sulfur capping of mortar cores



Figures 24 and 25: Cylinder core testing machine and placement of mortar core into apparatus



Figures 26 and 27: 4x8 concrete cylinder setup and failure mode



5 Testing and Evaluation Results

5.1. RESULTS AND OBSERVATIONS

Floor/Roof Flexural Test Results

In total, 12 floor/roof flexural tests were performed. Below is a list of the test parameters:

Wall lengths:	96.0 inches and 144 inches
Wall width:	48.0 inches
Nominal wall thicknesses:	7.5 inches (PSM80) and 9.5 inches (PSM150)
Initial pre-load:	Approx 1130 lbs (stand-by pressure of hydraulic pump)
Support Span (L):	93 inches (8 foot wall) and 141 inches (12 foot wall)
End Bearings:	3.0 inches
Load Bearings:	3.0 inches

The results obtained for the floor/roof flexural tests are tabulated as followed:

Specimen ID	Date Tested	Age of Wall (days)	*Ultimate Load (lbs)	Average (Ibs)	Average within 15%?	Allowable Load (lbs)
80_4X8FRF1	11/19/07	50	*10110			
80_4X8FRF2	11/19/07	50	*9520	9823	YES	9823
80_4X8FRF3	11/20/07	51	*9840			
80_4X12FRF1	11/27/07	55	*5730			
80_4X12FRF2	11/27/07	55	*5600	5593	YES	5593
80_4X12FRF3	11/28/07	56	*5450			
150_4X8FRF1	11/20/07	51	*12240			
150_4X8FRF2	11/21/07	52	*11890	11717	YES	11717
150_4X8FRF3	11/21/07	52	*11020			
150_4X12FRF1	11/28/07	56	*7160			
150_4X12FRF2	11/28/07	56	*6680	6770	YES	6770
150_4X12FRF3	11/29/07	57	*6470			

*NOTE: <u>The loads reported are for the hydraulic cylinder only and **DO NOT** take account for the weight of each specimen. All floor/roof flexural tests were performed in the horizontal position.</u>

The <u>Allowable Load</u> for each set of three samples was calculated under the guidelines of AC 15, Section 4.3, Paragraph 2, which states the following:

"The average maximum strength from each set of tests may be the average ultimate value, provided the ultimate value for each test is within 15 percent of the average. Otherwise, the lowest ultimate value shall be used."



Refer to Appendix A for Load vs. Deflection curves for all floor/roof flexural tests.

Transverse testing was performed according to Section 4.2.2.6 of ICC – AC 15, under the general guidelines of Section 11 of ASTM E 72-05. Each of the targeted deflection loads (L/360, L/240, L/180, L/120) were calculated by dividing the support span (L) by each load increment. The <u>mid-span mean</u> for each specimen was calculated by subtracting the average of the outer four dials from the lateral (middle) dials:

Mid-Span Mean = Average Lateral (Middle) Dials – Average Outer Dials

The Stiffness (EI) for each specimen was calculated from the maximum deflection equation of a simply-supported beam under third-point loading conditions. The maximum deflection used in the calculation was the maximum deflection recorded at the last target load obtained.

Stiffness EI = [23 * P * (L^3)] / (648 * Max Deflection)

Statistical analysis calculations were computed using the linear regression analysis method included in Microsoft Excel[®] (command "LINEST").

A CD copy of all the assembly, setup, and test photos will be provided to the client.



6 Conclusion

Intertek Testing Services NA, Inc. (Intertek) has conducted testing for Emmedue S.P.A on 4' x 8' and 4' x 12' Single Polystyrene PSM80 and PSM150 structural wall panels. The test method consisted of the transverse-flexural load under third-point loading. The purpose of these tests was to evaluate flexural load structural applications according to Section 4.2.2.6 of ICC – AC 15, under the general guidelines of *ASTM E 72 - 05, Conducting Strength Tests of Panels for Building Construction.* The results of each test were presented in tabular and graphical form. In total, 12 specimens were tested under the above loading configuration to measure the deflection and failure characteristics of each of the wall systems. This evaluation began November 19, 2007 and was completed November 29, 2007.

The conclusions of this test report may be used as part of the requirements for Intertek product certification. Authority to Mark must be issued for a product to become certified.

INTERTEK TESTING SERVICES NA, INC

Reported by:

Victor M. Burgos Test Engineer

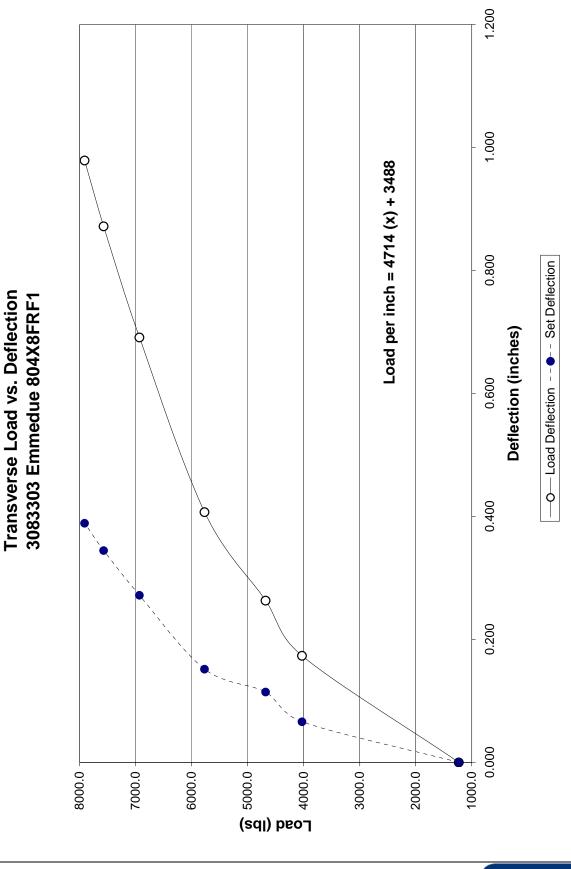
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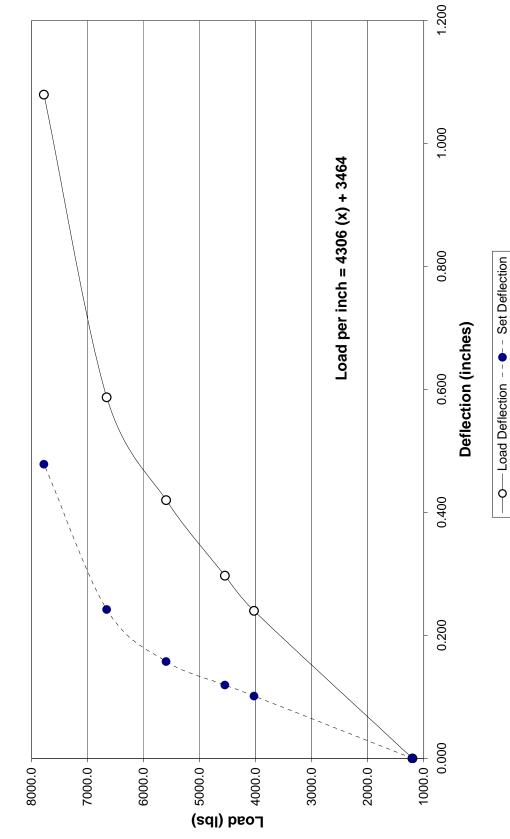
Michael E. Luna, M.S. General Manager



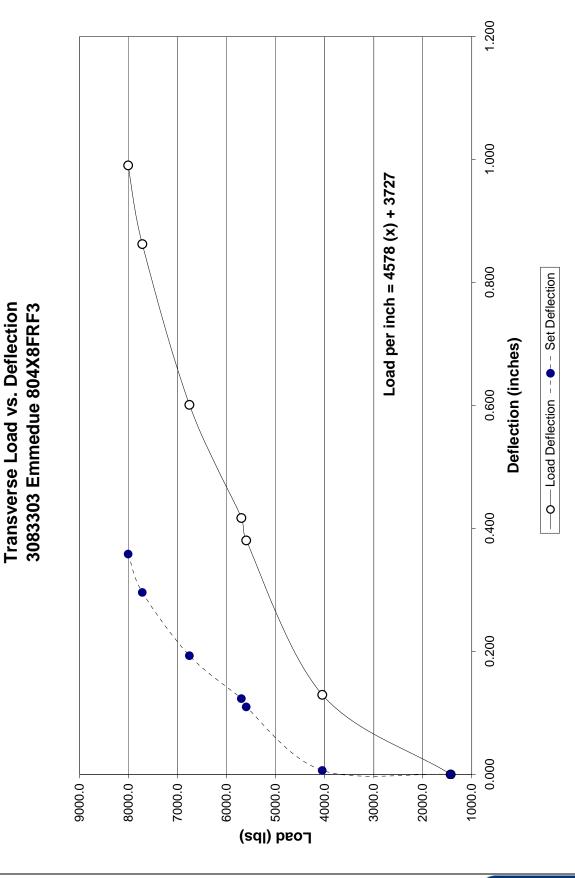
APPENDIX A Graphs



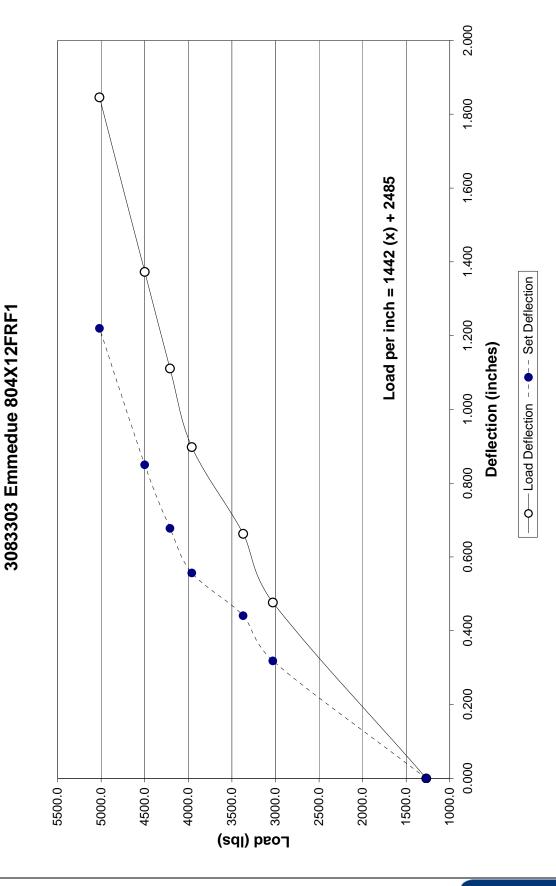




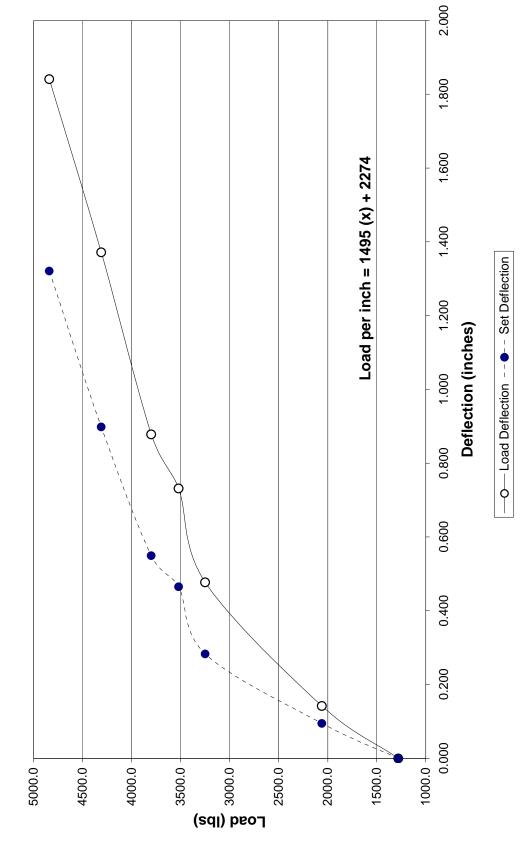


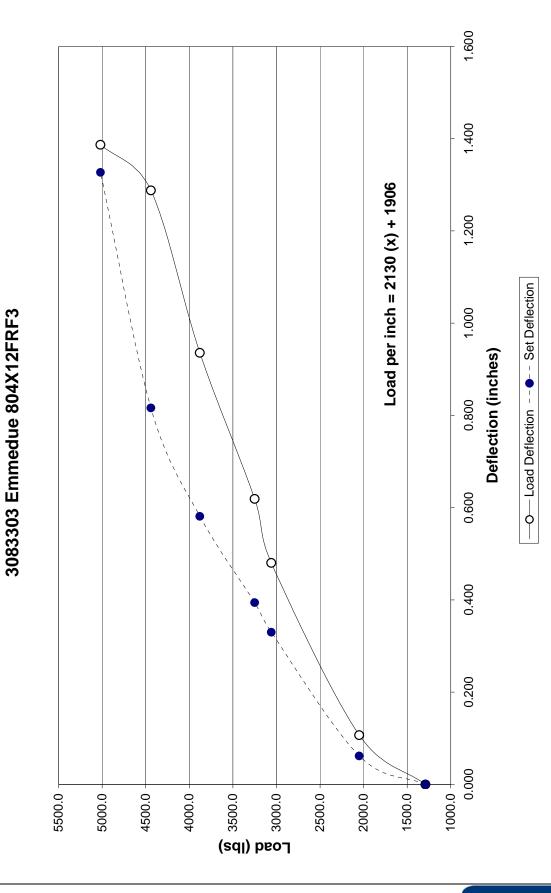


Emmedue



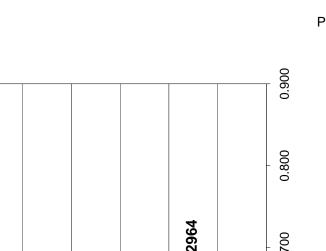
Transverse Load vs. Deflection



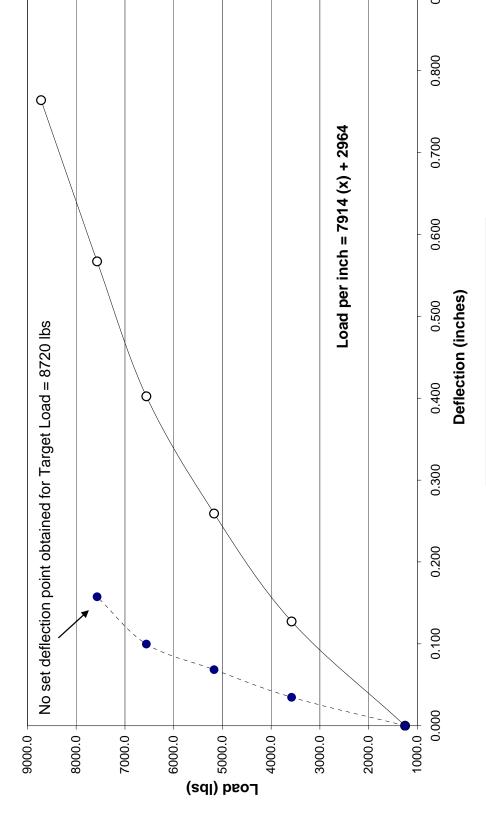




Transverse Load vs. Deflection

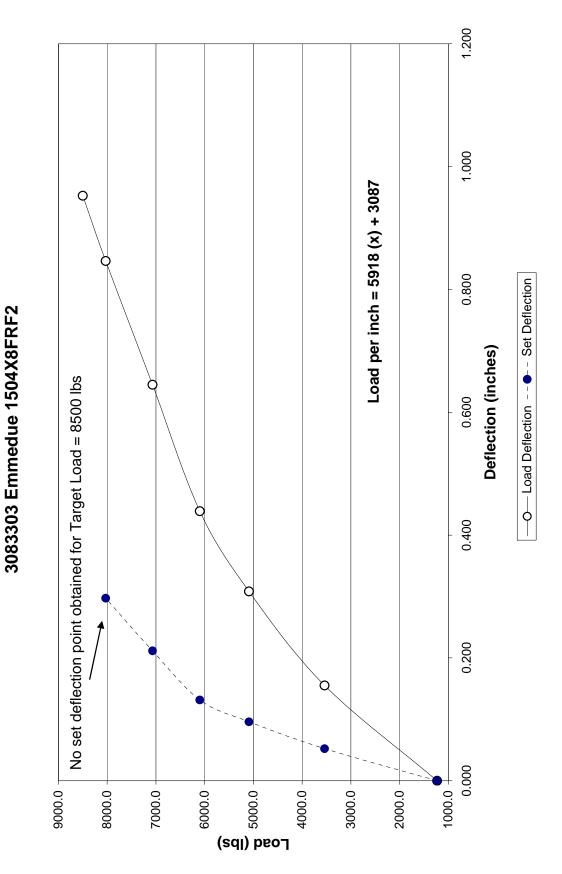


Transverse Load vs. Deflection 3083303 Emmedue 1504X8FRF1

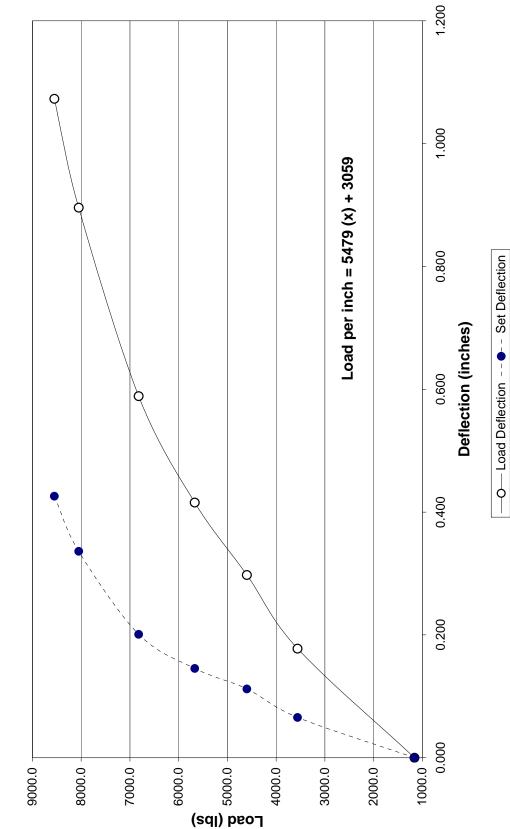


Set Deflection

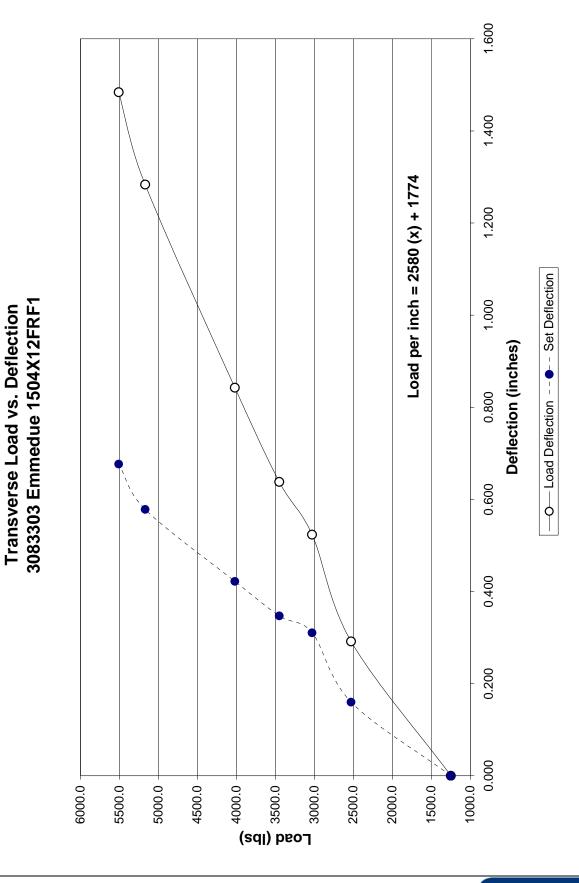
-O--- Load Deflection -- ----



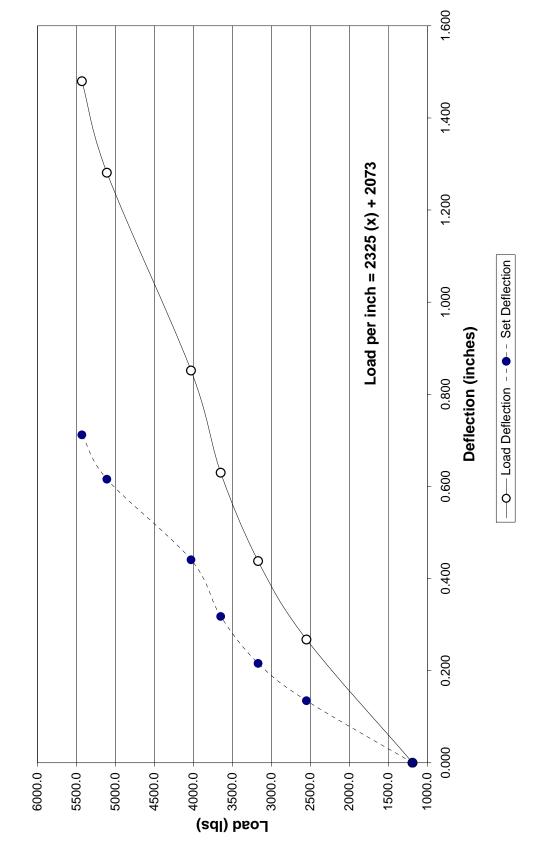
Transverse Load vs. Deflection



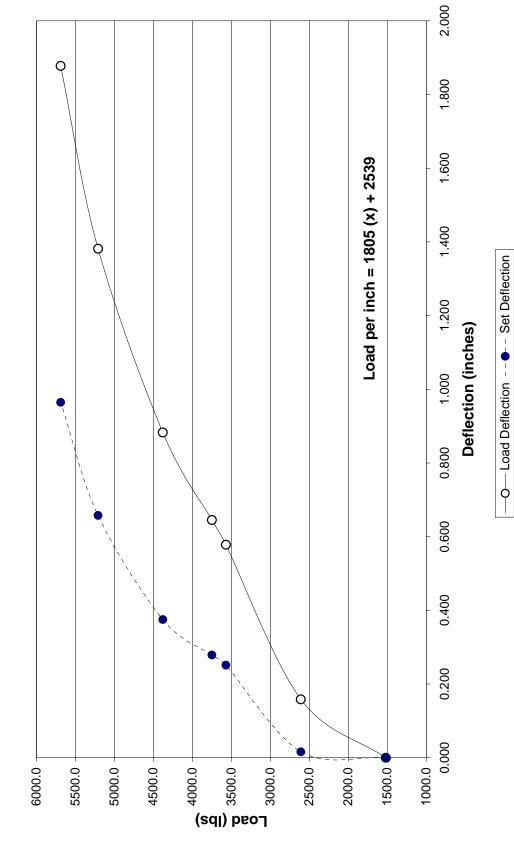
Transverse Load vs. Deflection 3083303 Emmedue 1504X8FRF3







Transverse Load vs. Deflection 3083303 Emmedue 1504X12FRF2



Transverse Load vs. Deflection 3083303 Emmedue 1504X12FRF3

APPENDIX B Test Data



Intertek

11/19/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_804X8FRF1 Single Polystyrene PSM80 4' x 8' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

g/m

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 32.00

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

1230 50 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 31 inches apart

Support Span		Panel		
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)
93	7.750	4.0	8.0	7.500

Transverse Flexural Load - Specimen Horizontal

		Outer Corner Measurements			Lateral Mea	asurements		
Piston Load (lbs)	Time	Trans 1 (in.)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan
Piston Load (IDS)	Time	Trans T (in.)	(in.)	Trans 5 (in.)	(in.)	(in.)	(in.)	Mean (in.)
1230	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4030	immed.	0.005	0.007	0.001	0.002	0.148	0.141	0.141
4030	~5min	0.005	0.008	0.001	0.002	0.182	0.172	0.173
1420	immed.	0.002	0.006	0.000	0.001	0.073	0.070	0.069
1410	~5min	0.003	0.006	0.001	0.001	0.070	0.068	0.066
4700	immed.	0.005	0.010	0.000	0.002	0.266	0.252	0.255
4680	~5min	0.004	0.010	0.000	0.002	0.274	0.260	0.263
1410	immed.	0.002	0.009	0.000	0.001	0.125	0.118	0.119
1390	~5min	0.002	0.008	0.000	0.000	0.120	0.114	0.114
5780	immed.	0.005	0.012	0.000	0.003	0.402	0.386	0.389
5770	~5min	0.005	0.012	0.000	0.003	0.420	0.404	0.407
1430	immed.	0.002	0.008	0.000	0.001	0.168	0.160	0.161
1410	~5min	0.003	0.009	0.000	0.002	0.159	0.151	0.152
6930	immed.	0.006	0.013	-0.004	0.005	0.664	0.650	0.652
6930	~5min	0.006	0.014	-0.004	0.004	0.708	0.684	0.691
1460	immed.	0.004	0.010	-0.004	0.004	0.305	0.288	0.293
1410	~5min	0.004	0.011	-0.003	0.004	0.284	0.268	0.272
7590	immed.	0.005	0.015	-0.005	0.007	0.848	0.814	0.826
7570	~5min	0.005	0.016	-0.005	0.007	0.896	0.859	0.872
1440	immed.	0.004	0.014	-0.004	0.004	0.380	0.360	0.366
1400	~5min	0.004	0.014	-0.004	0.004	0.359	0.339	0.345
7930	immed.	0.006	0.018	-0.008	0.006	0.960	0.920	0.935
7910	~5min	0.005	0.018	-0.010	0.006	1.004	0.963	0.979
1470	immed.	0.004	0.016	-0.004	0.004	0.435	0.412	0.419
1410	~5min	0.004	0.016	-0.005	0.004	0.405	0.382	0.389
			ULTI	MATE FAILURI	E DATA			
8160	Hold 2 min	Some popping	heard, no	visible damage				
8560	Hold 2 min	No change, no	visible dar	nage				
9120	Hold 2 min	No change, no	visible dar	nage				
9730	Hold 2 min	Cracking and p	popping he	ard between 15			id, no visible	damage
				Pan	el Failure	9		
	Wall no long	er able to hold I	oad. Failur	e occurred appi	ox 35 seco	nds into hold	ing load	
10110	Complete ho	orizontal shear f	ailure appr	oximately 41 inc	hes from le	ft bearing en	d (concrete,	mortar, wire m
	Horizontal fa	ontal failure is categorized as the length of the panel width (4 ft)						
	Cracks visib	le from RHS be	aring end u	ip to 30" on mor	tar underne	ath wall		
	No additiona	I visible damag	e present					

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Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen

*All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 4030 lbs, some popping heard approx 2.5 minutes into load, no visible damage present *At Load = 6930 lbs, some cracking and popping heard while taking wall to this load. Crack formation on mortar (lower side) at right end bearing location (photos taken). No additional visible damage present

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward

*The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

*Ruben Caputo, Emmedue consultant, present during testing

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1230.0	4920.0	0.000	0.0000	0.000
4030.0	16120.0	0.173	0.0144	0.066
4680.0	18720.0	0.263	0.0219	0.114
5770.0	23080.0	0.407	0.0339	0.152
6930.0	27720.0	0.691	0.0576	0.272
7570.0	30280.0	0.872	0.0727	0.345
7910.0	31640.0	0.979	0.0816	0.389

Stiffness (Flexural Rigidity) EI (Ibs-ft^2)	954607
Max Load (lbs)	10110

Intertek

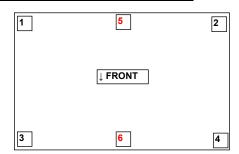
Client[.] Emmedue S P A Project No: M2_804X8FRF1 Product: Technician(s): Test Method(s):

Single Polystyrene PSM80 4' x 8' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Sup	oport Span		Panel	
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)
93	7.750	4.00	8.00	7.500

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	7141.52
L/ 180	5923.80
L/ 240	5314.94
L/ 360	4706.08



Linear Regression Analysis

4713.76477 3488.35588 357.424824 228.933238 0.97751884 265.288039 173.926753 4 12240572.4 281510.974

Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 4713.76

3488.36

+

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

Intertek

11/19/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_804X8FRF2 Single Polystyrene PSM80 4' x 8' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

glad)

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 32.00 1200

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

50 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 31 inches apart

Support Span		Panel		
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)
93	7.750	4.0	8.0	7.500

Transverse Flexural Load - Specimen Horizontal

		Outer Corner Measurements		Lateral Measurements				
Piston Load (lbs)	Time	Trans 1 (in.)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan
riston Load (ibs)	Time	mans r (m.)	(in.)	mans s (m.)	(in.)	(in.)	(in.)	Mean (in.)
1200	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3960	immed.	-0.002	0.015	0.012	0.010	0.221	0.227	0.215
4030	~5min	-0.002	0.016	0.012	0.011	0.246	0.252	0.240
1350	immed.	-0.002	0.010	0.008	0.005	0.110	0.112	0.106
1340	~5min	-0.001	0.010	0.008	0.006	0.106	0.108	0.102
4540	immed.	-0.002	0.013	0.010	0.010	0.290	0.296	0.285
4550	~5min	-0.002	0.014	0.011	0.010	0.302	0.308	0.297
1360	immed.	-0.002	0.010	0.008	0.006	0.129	0.131	0.124
1340	~5min	-0.002	0.010	0.008	0.006	0.124	0.126	0.119
5620	immed.	-0.002	0.018	0.014	0.012	0.410	0.416	0.402
5600	~5min	-0.002	0.018	0.014	0.013	0.429	0.433	0.420
1400	immed.	-0.002	0.010	0.010	0.008	0.175	0.176	0.169
1360	~5min	-0.002	0.011	0.010	0.007	0.163	0.165	0.158
6660	immed.	-0.002	0.024	0.016	0.017	0.543	0.548	0.532
6660	~5min	-0.004	0.026	0.020	0.022	0.605	0.601	0.587
1420	immed.	-0.003	0.014	0.010	0.004	0.268	0.264	0.260
1380	~5min	-0.003	0.014	0.010	0.005	0.250	0.247	0.242
7780	immed.	-0.004	0.031	0.024	0.022	0.949	0.915	0.914
7780	~5min	-0.005	0.029	0.026	0.020	1.113	1.081	1.080
1470	immed.	-0.005	0.016	0.012	0.003	0.538	0.502	0.514
1380	~5min	-0.004	0.016	0.011	0.002	0.502	0.468	0.479
			ULTI	MATE FAILURI	E DATA			
8120	Hold 2 min	nin Some cracking and popping heard, no visible damage						
8610	Hold 2 min	No change, no visible damage						
9100	Hold 2 min	No change, no	No change, no visible damage					
		Panel Failure						
	Wall no long	per able to hold load. Failure occurred approx 10 seconds into holding load prizontal shear failure approximately 38 inches from left bearing end (concrete, mortar, wire mesh) ailure is categorized as the length of the panel width (4 ft)						
9520	Complete ho							
	Horizontal fa							
	Cracks visib	ible from LHS bearing end between 30" and 48" on mortar underneath wall						
	No additiona	nal visible damage present						

Emmedue Project No. 3083303SAT - 004 REV1

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen

*All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 3960 lbs, some popping heard approx, no visible damage present

*At Load = 6660 lbs, popping heard approx. 1:20 into load, surface crack on bottom left mortar side (photos)

*At Load = 7780 lbs, additional cracking and popping heard. Wall continuing to deflect passing L/100

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward

*The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

*Ruben Caputo, Emmedue consultant, present during testing

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1200.0	4800.0	0.000	0.0000	0.000
4030.0	16120.0	0.240	0.0200	0.102
4550.0	18200.0	0.297	0.0248	0.119
5600.0	22400.0	0.420	0.0350	0.158
6660.0	26640.0	0.587	0.0489	0.242
7780.0	31120.0	1.080	0.0900	0.479

Stiffness (Flexural Rigidity) El (Ibs-ft^2)	790809
Max Load (lbs)	9520

Intertek

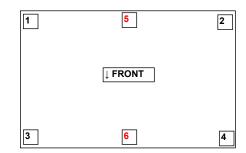
Client[.] Emmedue S P A Project No: M2_804X8FRF2 Product: Technician(s): Test Method(s):

Single Polystyrene PSM80 4' x 8' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Sup	port Span	Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
93	7.750	4.00	8.00	7.500	

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	6801.24
L/ 180	5688.80
L/ 240	5132.59
L/ 360	4576.37



Linear Regression Analysis

4306.21023 3463.92862 820.37588 496.689984 0.90180911 553.686706 27.5527335 3 8446813.09 919706.907

Equation of Best Fit Line Load (lbs-in) = Defl. (in) x 4306.21

3463.93

+

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

11/20/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_804X8FRF3 Single Polystyrene PSM80 4' x 8' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

glad .

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 32.00 1430

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

51 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 31 inches apart

Support Span		Panel				
(in)	(ft)	Width (ft) Length (ft) Thic		Thickness (in)		
93	7.750	4.0	8.0	7.500		

		Out	er Corner	Measurements		Lateral Mea	asurements	
Distant sad (lbs)	Times	Turner ((in)	Trans 2	Trans 0 (in)	Trans 4	Trans 5	Trans 6	Midspan
Piston Load (lbs)	Time	Trans 1 (in.)	(in.)	Trans 3 (in.)	(in.)	(in.)	(in.)	Mean (in.)
1430	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
4060	immed.	0.018	0.000	0.000	0.020	0.130	0.138	0.125
4050	~5min	0.018	0.001	0.000	0.020	0.136	0.143	0.129
1440	immed.	0.002	0.000	0.000	0.003	0.009	0.010	0.009
1440	~5min	0.002	0.000	0.000	0.002	0.007	0.008	0.006
5610	immed.	0.026	-0.001	0.002	0.026	0.350	0.357	0.340
5600	~5min	0.028	-0.001	0.002	0.026	0.393	0.396	0.381
1440	immed.	0.010	-0.002	-0.003	0.019	0.118	0.128	0.117
1430	~5min	0.009	-0.001	-0.003	0.019	0.111	0.120	0.110
5720	immed.	0.026	-0.001	-0.002	0.020	0.412	0.416	0.403
5700	~5min	0.026	-0.002	-0.002	0.020	0.424	0.431	0.417
1460	immed.	0.011	-0.001	-0.005	0.019	0.130	0.145	0.131
1440	~5min	0.011	-0.001	-0.005	0.019	0.122	0.137	0.123
6720	immed.	0.030	-0.002	-0.001	0.021	0.555	0.564	0.547
6760	~5min	0.032	-0.002	0.000	0.023	0.608	0.620	0.601
1520	immed.	0.017	-0.004	-0.008	0.023	0.210	0.231	0.213
1440	~5min	0.016	-0.004	-0.008	0.024	0.189	0.211	0.193
7730	immed.	0.030	-0.010	-0.006	0.024	0.807	0.820	0.804
7720	~5min	0.030	-0.010	-0.007	0.023	0.868	0.875	0.863
1480	immed.	0.018	-0.013	-0.012	0.024	0.310	0.328	0.315
1440	~5min	0.018	-0.013	-0.013	0.024	0.291	0.309	0.296
8010	immed.	0.023	-0.013	-0.008	0.024	0.968	0.946	0.950
8010	~5min	0.023	-0.012	-0.006	0.024	1.010	0.985	0.991
1510	immed.	0.014	-0.013	-0.010	0.024	0.394	0.380	0.383
1440	~5min	0.013	-0.014	-0.012	0.024	0.368	0.355	0.358
			ULTI	MATE FAILURI	DATA			
8590	Hold 2 min	Some popping	heard, no	visible damage				
9140	Hold 2 min	No change, no	visible da	mage				
9600	Hold 2 min	No change, no	visible da					
				Pan	el Failure	9		
	Wall no long	er able to hold load. Failure occurred approx 5 seconds into holding load						
9840	Complete ho	rizontal shear failure approximately 43 inches from left bearing end (concrete, mortar, wire me						
				length of the pa			. ,	
	Cracks visib	le from LHS bea	aring end b	etween 30" and	52" on moi	rtar undernea	ath wall	
		al visible damag						

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 5600 lbs, some popping and cracking heard, wall settling at this load (deflections more apparent) *At Load = 6760 lbs, some cracking and popping heard approx. 20 seconds into load, second pop at 1:15 No visible damage present

*At Load = 8010 lbs, pop heard. Two cracks visible at lower midspan, approx 8" apart (photos taken)

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

*Ruben Caputo, Emmedue consultant, present during testing

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1430.0	5720.0	0.000	0.0000	0.000
4050.0	16200.0	0.129	0.0108	0.006
5600.0	22400.0	0.381	0.0317	0.110
5700.0	22800.0	0.417	0.0348	0.123
6760.0	27040.0	0.601	0.0501	0.193
7720.0	30880.0	0.863	0.0719	0.296
8010.0	32040.0	0.991	0.0825	0.358

Stiffness (Flexural Rigidity) EI (lbs-ft ²)	916400
Max Load (Ibs)	9840

Load achieved within 1 minute

Intertek

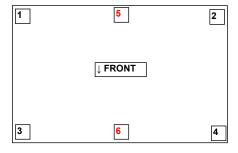
Client: Emmedue S.P.A Project No: M2_804X8FRF3 Product: Single Polystyrene PSM80 4' x 8' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) Technician(s): V. Burgos, Intertek San Antonio ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Test Method(s): Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05

Sup	Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)		
93	7.750	4.00	8.00	7.500		

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	7274.89
L/ 180	6092.18
L/ 240	5500.82
L/ 360	4909.46



4578.26 3726.74085 339.459367 215.66647 0.9784827 243.964449 181.896906 4 10826258.7 238074.61



Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 4578.26+

3726.74

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

11/27/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_804X12FRF1 Single Polystyrene PSM80 4' x 12' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

g/m

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 48.00 1270

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

55 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 47 inches apart

Support Span		Panel				
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)		
141	11.750	4.0	12.0	7.500		

		Outer Corner Measurements Lateral Measurements						
Piston Load (lbs)	Time	Trans 1 (in.)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan
Fiston Load (ibs)	Time	Trans T (III.)	(in.)	Trans 5 (III.)	(in.)	(in.)	(in.)	Mean (in.)
1270	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2930	immed.	0.005	0.002	0.000	0.012	0.306	0.292	0.294
3030	~5min	0.008	0.003	0.000	0.016	0.494	0.473	0.477
1570	immed.	0.006	0.001	0.000	0.014	0.332	0.320	0.321
1570	~5min	0.005	0.002	0.000	0.014	0.330	0.318	0.319
3340	immed.	0.008	0.003	-0.002	0.018	0.597	0.577	0.580
3370	~5min	0.009	-0.002	-0.002	0.020	0.680	0.659	0.663
1580	immed.	0.008	-0.005	-0.002	0.017	0.459	0.446	0.448
1570	~5min	0.008	-0.005	-0.002	0.017	0.452	0.439	0.441
3870	immed.	0.010	-0.001	-0.001	0.022	0.843	0.821	0.824
3960	~5min	0.010	-0.001	-0.002	0.024	0.918	0.893	0.898
1660	immed.	0.008	-0.004	-0.002	0.020	0.595	0.579	0.581
1570	~5min	0.008	-0.005	-0.002	0.020	0.570	0.555	0.557
4140	immed.	0.010	-0.002	-0.001	0.025	0.988	0.961	0.967
4210	~5min	0.011	0.000	-0.001	0.027	1.135	1.106	1.111
1630	immed.	0.009	-0.005	-0.001	0.022	0.709	0.698	0.697
1570	~5min	0.010	-0.006	-0.002	0.022	0.690	0.679	0.678
4530	immed.	0.012	-0.003	-0.002	0.028	1.264	1.233	1.240
4500	~5min	0.012	-0.004	-0.002	0.028	1.400	1.364	1.373
1640	immed.	0.013	-0.006	-0.002	0.025	0.888	0.868	0.870
1580	~5min	0.013	-0.006	-0.002	0.025	0.866	0.848	0.850
4880	immed.	0.014	-0.003	-0.003	0.030	1.600	1.559	1.570
5020	~5min	0.015	-0.004	-0.012	0.032	1.857	1.851	1.846
1650	immed.	0.012	-0.008	-0.014	0.027	1.256	1.237	1.242
1590	~5min	0.013	-0.008	-0.013	0.026	1.234	1.216	1.220
			ULTI	MATE FAILURE	DATA			
5450	Hold 2 min	Popping heard	, wall inspe	ected, no visual	damage			
0		0						
	Woll no long	or oble to held !	and Failur		el Failure		holding lood	
5720		ger able to hold load. Failure occurred approx 10 - 15 seconds into holding load						
5730		prizontal shear failure approximately 63 inches from right bearing end (concrete, mortar, wire mes hear failure is described as the complete break along the panel 4 ft width						
					0		twidth	
				slow deflection u	until failure)			
	No additiona	al visible damag	e present					

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Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen

*All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 3030 lbs, several pops heard while taking wall to this load, no visible damage present

*At Load = 3370 lbs, two pops heard while taking wall to this load, no visible damage

*At Load = 3960 lbs, load had to be slightly adjusted. Load stabalized after 1 minute

*At Load = 4210 lbs, additional popping heard approx 1.5 minutes into load, no visual damage

*At Load = 4500 lbs, Transducer 4 showing more deflection than others, no visual damage present at location

*At Load = 5020 lbs, pops heard approx 30 seconds into load, no visual damage

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward

*The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1270.0	5080.0	0.000	0.0000	0.000
3030.0	12120.0	0.477	0.0397	0.319
3370.0	13480.0	0.663	0.0553	0.441
3960.0	15840.0	0.898	0.0748	0.557
4210.0	16840.0	1.111	0.0926	0.678
4500.0	18000.0	1.373	0.1144	0.850
5020.0	20080.0	1.846	0.1539	1.220

Stiffness (Flexural Rigidity) El (lbs-ft^2)	539544
Max Load (lbs)	5730

Intertek

Client: Emmedue S.P.A Project No: M2_804X12FRF1 Product: Single Polystyrene PSM80 4' x 12' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) Technician(s): V. Burgos, Intertek San Antonio ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Test Method(s):

Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Support Span		Panel				
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)		
141	11.750	4.00	12.00	7.500		

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	4178.70
L/ 180	3614.05
L/ 240	3331.73
L/ 360	3049.41

Linear Regression Analysis

1441.64346 2484.76755 134.682565 155.543172 0.96626631 150.12909 114.575819 4 2582395.03 90154.9749

2 1 5 FRONT 3 6 4

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

Equation of Best Fit Line Load (lbs-in) = Defl. (in) x 1441.64

2484.77

+

11/27/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_804X12FRF2 Single Polystyrene PSM80 4' x 12' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

e ha

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 48.00

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

55 days (at test date) Third-Point Loading

1280

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 47 inches apart

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
141	11.750	4.0	12.0	7.500	

Transverse Flexural Load - Specimen Horizontal

		Out	ter Corner	Measurements	6	Lateral Mea	surements	
Piston Load (Ibs)	Time	Trans 1 (in.)	Trans 2 (in.)	Trans 3 (in.)	Trans 4 (in.)	Trans 5 (in.)	Trans 6 (in.)	Midspan Mean (in.)
1280	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2050	immed.	0.002	0.000	-0.001	0.006	0.099	0.097	0.096
2060	~5min	0.002	0.000	-0.001	0.009	0.150	0.140	0.142
1510	immed.	0.003	0.000	-0.001	0.010	0.108	0.096	0.099
1450	~5min	0.002	0.000	-0.001	0.009	0.103	0.092	0.095
3220	immed.	0.003	-0.001	-0.001	0.014	0.424	0.397	0.407
3250	~5min	0.004	-0.001	0.000	0.016	0.496	0.467	0.477
1570	immed.	0.004	-0.002	-0.001	0.016	0.310	0.292	0.297
1510	~5min	0.004	-0.002	0.000	0.016	0.297	0.278	0.283
3590	immed.	0.008	-0.008	-0.002	0.018	0.695	0.676	0.682
3520	~5min	0.008	-0.009	-0.002	0.018	0.743	0.728	0.732
1590	immed.	0.008	-0.008	-0.002	0.018	0.492	0.482	0.483
1520	~5min	0.008	-0.009	-0.002	0.018	0.474	0.464	0.465
3800	immed.	0.008	-0.008	-0.002	0.020	0.817	0.802	0.805
3800	~5min	0.008	-0.011	-0.002	0.020	0.893	0.872	0.878
1570	immed.	0.009	-0.012	-0.004	0.020	0.577	0.561	0.566
1510	~5min	0.009	-0.012	-0.004	0.020	0.561	0.545	0.550
4360	immed.	0.011	-0.019	-0.007	0.020	1.271	1.243	1.256
4310	~5min	0.012	-0.022	-0.010	0.020	1.388	1.356	1.372
1660	immed.	0.012	-0.022	-0.015	0.020	0.949	0.928	0.940
1520	~5min	0.012	-0.022	-0.016	0.020	0.906	0.888	0.899
4790	immed.	0.010	-0.026	-0.014	0.020	1.808	1.654	1.734
4840	~5min	0.005	-0.028	-0.014	0.019	2.004	1.670	1.841
1660	immed.	0.006	-0.021	-0.017	0.020	1.378	1.338	1.361
1530	~5min	0.006	-0.021	-0.017	0.020	1.338	1.299	1.321
			ULTI	MATE FAILURI	E DATA			
5040	Hold 2 min	No cracks or p	ops, no vis	ible damage				
0		0	1 '	0				
5600	Complete ho Horizontal sl	orizontal shear f hear failure is d	ailure appr escribed as	Pan re occurred appr oximately 82 inc s the complete b slow deflection	hes from ri reak along	nds into hold ght bearing e the panel 4 f	nd (concrete	e, mortar, wir

No additional visible damage present

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 3520 lbs, one loud pop heard, wall settled. Transducers 5 & 6 showed significant movement at approximately 1:20 into load. No visible damage present

*At Load = 4310 lbs, additional pop heard. Crack formation on lower RHS mortar, approx 55" - 58" from the

right end. Photos taken. The crack was found the be larger underneath wall at Transducer 5 location

*At Load = 4840 lbs, one loud pop heard, no visual damage

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1280.0	5120.0	0.000	0.0000	0.000
2060.0	8240.0	0.142	0.0119	0.095
3250.0	13000.0	0.477	0.0398	0.283
3520.0	14080.0	0.732	0.0610	0.465
3800.0	15200.0	0.878	0.0732	0.550
4310.0	17240.0	1.372	0.1143	0.899
4840.0	19360.0	1.841	0.1534	1.321

Stiffness (Flexural Rigidity) EI (lbs-ft ²)	560856
Max Load (Ibs)	5600

Intertek

141

Client: Emmedue S.P.A Project No: M2_804X12FRF2 Product: Single Polystyrene PSM80 4' x 12' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) Technician(s): V. Burgos, Intertek San Antonio Test Method(s): ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05

Load achieved within 1 minute Support Span Panel Width (ft) Length (ft) Thickness (in) (in) (ft)

4.00

Deflection Limit (L/x)	Load (Ibs-in)	1	5	2
L/ 120	4030.28			
L/ 180	3444.89			
L/ 240	3152.20			
L/ 360	2859.50		↓ FRONT	

1Ľ

12.00

0.92250227 297.77995 47 6144175 4 4222108.41 354691.594

11.750

Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 1494.612274.11 +

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

7.500

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

11/28/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_804X12FRF3 Single Polystyrene PSM80 4' x 12' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

g/m

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 48.00 1290

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

56 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 47 inches apart

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
141	11.750	4.0	12.0	7.500	

		Out	er Corner	Measurements		Lateral Mea	asurements		
Piston Load (lbs)	Time	Trans 1 (in.)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan	
r istoir Eoad (ibs)	Time	Trans T (iii.)	(in.)	Trans 5 (III.)	(in.)	(in.)	(in.)	Mean (in.)	
1290	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
2030	immed.	0.000	0.001	0.005	0.001	0.081	0.090	0.084	
2050	~5min	0.000	0.001	0.005	0.003	0.103	0.116	0.107	
1510	immed.	0.000	0.001	0.005	0.003	0.062	0.072	0.065	
1500	~5min	0.000	0.002	0.004	0.003	0.059	0.069	0.062	
3190	immed.	0.000	0.007	0.009	0.011	0.400	0.425	0.406	
3060	~5min	0.000	0.008	0.009	0.015	0.479	0.498	0.481	
1600	immed.	-0.001	0.007	0.007	0.015	0.341	0.356	0.341	
1550	~5min	-0.001	0.006	0.007	0.015	0.330	0.344	0.330	
3220	immed.	-0.001	0.007	0.008	0.015	0.604	0.621	0.605	
3250	~5min	-0.001	0.007	0.007	0.015	0.617	0.636	0.619	
1660	immed.	-0.001	0.004	0.006	0.015	0.412	0.426	0.412	
1580	~5min	-0.001	0.004	0.006	0.015	0.394	0.408	0.394	
3840	immed.	-0.002	0.010	0.006	0.020	0.865	0.886	0.867	
3880	~5min	-0.002	0.009	0.016	0.020	0.932	0.962	0.936	
1690	immed.	-0.002	0.004	0.018	0.020	0.605	0.630	0.607	
1590	~5min	-0.003	0.004	0.017	0.020	0.579	0.603	0.582	
4400	immed.	-0.003	0.006	0.022	0.020	1.173	1.212	1.181	
4440	~5min	-0.005	0.004	0.022	0.023	1.276	1.322	1.288	
1720	immed.	-0.006	-0.004	0.023	0.023	0.844	0.872	0.849	
1620	~5min	-0.006	-0.004	0.022	0.023	0.812	0.838	0.817	
4760	immed.	-0.006	0.000	0.023	0.023	1.361	1.424	1.382	
5020	~5min	-0.008	0.000	0.021	0.025	1.364	1.430	1.387	
1760	immed.	-0.010	-0.010	0.017	0.026	1.334	1.382	1.352	
1620	~5min	-0.010	-0.011	0.017	0.026	1.312	1.354	1.327	
			ULTI	MATE FAILURE	E DATA				
5220	Hold 2 min	No cracks or p	ops, no vis	ible damage					
5290	Hold 2 min	No change, no	visible dar						
				Pan	el Failure	e			
	Wall no long	er able to hold I	oad. Failur	e occurred appr	ox 5 secon	ds into holdir	ng load		
5450	Complete ho	orizontal shear fa	ailure appr	oximately 58.5 in	nches from	right bearing	end (concre	ete, mortar, wii	re mesh)
	Horizontal sl	hear failure is de	escribed as	the complete b	reak along	the panel 4 f	t width		
	Wall failed s	uddenly at targe	et load (no	slow deflection	until failure)	-			
	No additiona	al visible damage	e present		,				

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 3060 lbs, popping heard, wall settling, movement on all Transducers. No visible damage

*At Load = 3250 lbs, crack formation underneath wall (tension side) close to midspan. Photos taken

*At Load = <u>3880 lbs</u>, two loud pops heard. Crack formation underneath wall becoming larger, approx 68" - 69"

from right end (close to midspan of wall). Photos taken

*At Load = 4440 lbs, pop heard at 2:25 into load, movement on all Transducers. Midspan mortar crack growing *At Load = 5020 lbs, cracks and pops heard 1 minute into load. Midspan crack increasing in size (separation) *Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1290.0	5160.0	0.000	0.0000	0.000
2050.0	8200.0	0.107	0.0089	0.062
3060.0	12240.0	0.481	0.0401	0.330
3250.0	13000.0	0.619	0.0516	0.394
3880.0	15520.0	0.936	0.0780	0.582
4440.0	17760.0	1.288	0.1073	0.817
5020.0	20080.0	1.387	0.1156	1.327

Stiffness (Flexural Rigidity) El (lbs-ft^2)	1061043
Max Load (lbs)	5450

Intertek

Client: Emmedue S.P.A Project No: M2_804X12FRF3 Product: Single Polystyrene PSM80 4' x 12' x 7.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) Technician(s): V. Burgos, Intertek San Antonio Test Method(s):

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Sup	port Span		Panel	
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)
141	11.750	4.00	12.00	7.500

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	4409.04
L/ 180	3574.70
L/ 240	3157.53
L/ 360	2740.37

Linear Regression Analysis

2130.21898 1906.02982 139.183122 128.142331 0.98321075 153.522984 234.247709 4 5521056.11 94277.227

2 1 5 FRONT 3 6 4

Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 2130.22

1906.03

+

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Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

11/20/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_1504X8FRF1 Single Polystyrene PSM150 4' x 8' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

glad)

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 32.00 1250

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

51 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 31 inches apart

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
93	7.750	4.0	8.0	9.500	

		Outer Corner Measurements Lateral Measurements							
Piston Load (lbs)	Time	Trans 1 (in.)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan	
. ,		· · · · ·	(in.)		(in.)	(in.)	(in.)	Mean (in.)	
1250	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
3560	immed.	0.009	0.013	0.005	0.006	0.130	0.125	0.119	
3580	~5min	0.009	0.013	0.005	0.005	0.138	0.133	0.127	
1380	immed.	0.003	0.010	0.004	0.005	0.043	0.041	0.036	
1370	~5min	0.003	0.010	0.004	0.005	0.041	0.039	0.035	
5140	immed.	0.016	0.015	0.009	0.006	0.250	0.248	0.238	
5170	~5min	0.016	0.016	0.009	0.006	0.272	0.270	0.259	
1400	immed.	0.009	0.011	0.005	0.006	0.082	0.082	0.074	
1370	~5min	0.008	0.011	0.005	0.006	0.076	0.076	0.069	
6560	immed.	0.022	0.016	0.012	0.009	0.400	0.396	0.383	
6560	~5min	0.023	0.016	0.013	0.008	0.420	0.415	0.402	
1400	immed.	0.013	0.012	0.005	0.006	0.119	0.118	0.110	
1370	~5min	0.012	0.012	0.006	0.006	0.110	0.108	0.100	
7580	immed.	0.029	0.018	0.017	0.010	0.548	0.536	0.523	
7570	~5min	0.030	0.018	0.027	0.010	0.592	0.584	0.567	
1410	immed.	0.016	0.010	0.016	0.007	0.184	0.180	0.170	
1370	~5min	0.015	0.010	0.014	0.007	0.171	0.168	0.158	
8740	immed.	0.176	0.010	0.188	0.006	0.860	0.836	0.753	
8720	~5min	0.238	0.009	0.251	0.006	0.903	0.877	0.764	
0	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
0	~5min	0.000	0.000	0.000	0.000	0.000	0.000	0.000	
			ULTI	MATE FAILURI	E DATA				
8780	Hold 2 min	Crack getting I	arger, no a	dditional visible	damage				
10030	Hold 2 min	Some cracking	and poppi	ng heard 1:00 i	nto load, no	additional vi	sible damag	е	
				Pan	el Failure) 			
	Wall no long	er able to hold	load. Failur	e occurred appi	ox 10 seco	nds into hold	ing load		
12240	Horizontal sh	near failure app	roximately	31 inches from	right bearin	g end (concr	ete and mort	tar breaks)	
	Wall not fully	separated from	n wire mes	h and foam core	. Left end b	earing morta	ar/foam crusł	hing 9" - 10" fr	rom end.
	Right end be	aring mortar/fo	am crushin	g approx 6" fror	n end.	2		-	
	Foam core a	it both end bear	ing location	ns began to squ	ish down fir	st, the morta	r breaks the	n followed	

1/5/09 Page 46

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 7570 lbs, pop heard while taking wall to this load, no visual damage present

*At Load = 8720 lbs, wall slipped off roller reaction end bearings. Test was stopped.

Wall was repositioned and last load target obtained was repeated on 11/21/07. However, due to testing on the previous day, a mortar crack 9.5" - 10" from the left end bearing was found, fully extending the width of the wall.

Crack formed when wall specimen slipped off roller bearings the previous day. Photos taken prior to retesting. Load vs. deflection readings were recorded, however deflections were high due to wall damage. Transducers

were removed after the set load reading and wall was taken to Ultimate Failure.

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

*Ruben Caputo, Emmedue consultant, was present on 11/20/07

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1250.0	5000.0	0.000	0.0000	0.000
3580.0	14320.0	0.127	0.0106	0.035
5170.0	20680.0	0.259	0.0216	0.069
6560.0	26240.0	0.402	0.0335	0.100
7570.0	30280.0	0.567	0.0473	0.158
8720.0	34880.0	0.764	0.0637	0.000

Stiffness (Flexural Rigidity) EI (lbs-ft ²)	2053764
Max Load (Ibs)	12240
	-

Emmedue S.P.A

M2_1504X8FRF1

Intertek

Client: Project No: Product: Technician(s): Test Method(s):

Single Polystyrene PSM150 4' x 8' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

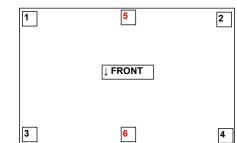
ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
93	7.750	4.00	8.00	9.500	

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	9097.55
L/ 180	7053.06
L/ 240	6030.82
L/ 360	5008.57
E/ 886	0000101

Linear Regression Analysis

7914.15636 2964.08114 767.70693 368.299829 0.97254554 385.158951 106.271872 3 15765157.7 445042.253



Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 7914.16

2964.08

+

11/21/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_1504X8FRF2 Single Polystyrene PSM150 4' x 8' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

g/m

Eng. Initials:

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 32.00 1230

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

52 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 31 inches apart

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
93	7.750	4.0	8.0	9.500	

Transverse Flexural Load - Specimen Horizontal

		Out	er Corner	Measurements	5	Lateral Mea	asurements	
Piston Load (lbs)	Time	Tropo 1 (in)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan
Piston Load (IDS)	Time	Trans 1 (in.)	(in.)	Trans 5 (III.)	(in.)	(in.)	(in.)	Mean (in.)
1230	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3530	immed.	0.002	0.010	0.000	0.002	0.154	0.140	0.144
3540	~5min	0.003	0.010	-0.001	0.002	0.166	0.151	0.155
1390	immed.	0.000	0.007	-0.001	0.001	0.062	0.052	0.055
1370	~5min	0.000	0.006	-0.002	0.000	0.058	0.049	0.052
5090	immed.	0.004	0.019	-0.003	0.004	0.304	0.281	0.287
5090	~5min	0.005	0.020	-0.003	0.004	0.328	0.302	0.308
1400	immed.	0.001	0.010	-0.004	0.002	0.111	0.100	0.103
1370	~5min	0.001	0.010	-0.003	0.002	0.104	0.093	0.096
6060	immed.	0.007	0.025	-0.004	0.006	0.425	0.401	0.405
6100	~5min	0.008	0.026	-0.006	0.008	0.456	0.440	0.439
1410	immed.	0.002	0.014	-0.005	0.003	0.153	0.146	0.146
1360	~5min	0.001	0.013	-0.005	0.003	0.138	0.131	0.132
7060	immed.	0.012	0.056	-0.010	0.009	0.582	0.555	0.552
7070	~5min	0.012	0.082	-0.014	0.060	0.687	0.673	0.645
1420	immed.	0.003	0.050	-0.012	0.035	0.253	0.244	0.230
1360	~5min	0.003	0.049	-0.013	0.034	0.234	0.226	0.212
8030	immed.	0.014	0.125	-0.018	0.120	0.836	0.827	0.771
8030	~5min	0.016	0.179	-0.020	0.166	0.936	0.928	0.847
1430	immed.	0.004	0.210	-0.025	0.186	0.423	0.414	0.324
1370	~5min	0.004	0.204	-0.025	0.180	0.393	0.384	0.297
8520	immed.	0.020	0.428	-0.029	0.367	1.146	1.124	0.939
8500	~5min	0.019	0.499	-0.032	0.440	1.197	1.172	0.953
0	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
0	~5min	0.000	0.000	0.000	0.000	0.000	0.000	0.000
			ULTI	MATE FAILURI	E DATA			
9030	Hold 2 min	No change, no	visible dar	nage				
10060	Hold 2 min	Some cracking	and poppi				sible damag	e
11890	Hold 2 min Some cracking and popping heard 1:10 into load, no additional visible damage Panel Failure Wall no longer able to hold load. Failure occurred approx 15 seconds into holding load Horizontal shear failure approximately 31 inches from right bearing end (concrete and mortar breaks) Wall not fully separated from wire mesh and foam core. Left end bearing mortar/foam crushing 9" from end. Right end bearing mortar/foam crushing approx 10" from end.							

Foam core at both end bearing locations began to squish down first, the mortar breaks then followed

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 7070 lbs, Transducers 2 & 4 (RHS end) showing movement due to foam crushing. Popping and cracking heard at 1:25 and 1:50 into load.

*At Load = 8030 lbs, Transducers 2 & 4 (RHS end) showing significant movement due to foam crushing approx 9" to 10" from right bearing end. Mortar crack formation at this location (photos taken)

*At Load = 8500 lbs, approximately 30 seconds into load, the end bearing crushing at right end of wall extended Wall shifted to right side and loading beam slipped off. Wall was repositioned, transducers were removed, and wall was taken to Ultimate Failure.

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1230.0	4920.0	0.000	0.0000	0.000
3540.0	14160.0	0.155	0.0129	0.052
5090.0	20360.0	0.308	0.0257	0.096
6100.0	24400.0	0.439	0.0366	0.132
7070.0	28280.0	0.645	0.0538	0.212
8030.0	32120.0	0.847	0.0705	0.297
8500.0	34000.0	0.953	0.0794	0.000

Stiffness (Flexural Rigidity) EI (lbs-ft ²)	1231415
Max Load (lbs)	11890

Intertek

Client: Emmedue S.P.A Project No: M2_1504X8FRF2 Product: Technician(s): Test Method(s):

Single Polystyrene PSM150 4' x 8' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

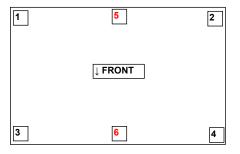
ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Support Span		Panel				
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)		
93	7.750	4.00	8.00	9.500		

Load (Ibs-in)
7673.50
6144.71
5380.32
4615.93

Linear Regression Analysis

5917.88937 3087.13738 508 969487 318 693857 0.97126266 354.585323 135.19175 4 16997760.3 502923.006



Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 5917.89

3087.14

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

11/21/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_1504X8FRF3 Single Polystyrene PSM150 4' x 8' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

Project #: 3083303

g/m

Eng. Initials:

 Test Method(s):
 ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05

 Wall Area (in^2):
 32.00

 Pre-Load (lbs)
 1160

Pre-Load (lbs)1160Age of Wall:52 days (at test date)Load Method:Third-Point LoadingBearing Type:1 inch diameter steel

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 31 inches apart

Support Span		Panel				
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)		
93	7.750	4.0	8.0	9.500		

		Out	Outer Corner Measurements Lateral Measurements					
Distant Lead (lbs)	Times	Turner A (in)	Trans 2	Trees O (in)	Trans 4	Trans 5	Trans 6	Midspan
Piston Load (lbs)	Time	Trans 1 (in.)	(in.)	Trans 3 (in.)	(in.)	(in.)	(in.)	Mean (in.)
1160	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
3550	immed.	0.003	0.008	0.000	0.011	0.173	0.174	0.168
3560	~5min	0.004	0.009	0.000	0.012	0.183	0.185	0.178
1310	immed.	0.002	0.006	-0.001	0.008	0.072	0.074	0.070
1310	~5min	0.002	0.006	0.000	0.007	0.071	0.067	0.066
4620	immed.	0.007	0.018	-0.001	0.018	0.303	0.291	0.286
4600	~5min	0.007	0.017	-0.001	0.019	0.314	0.302	0.298
1350	immed.	0.002	0.006	-0.001	0.014	0.126	0.119	0.118
1330	~5min	0.002	0.006	-0.002	0.013	0.121	0.113	0.112
5660	immed.	0.010	0.016	-0.001	0.022	0.413	0.398	0.394
5670	~5min	0.010	0.016	-0.002	0.023	0.436	0.419	0.416
1380	immed.	0.004	0.007	-0.001	0.017	0.168	0.160	0.157
1330	~5min	0.004	0.006	-0.001	0.017	0.156	0.148	0.146
6800	immed.	0.016	0.024	-0.004	0.028	0.571	0.542	0.541
6820	~5min	0.017	0.028	-0.004	0.030	0.624	0.590	0.589
1390	immed.	0.005	0.014	-0.004	0.020	0.236	0.218	0.218
1330	~5min	0.005	0.013	-0.005	0.020	0.218	0.200	0.201
8030	immed.	0.019	0.040	-0.007	0.032	0.828	0.799	0.793
8050	~5min	0.019	0.046	-0.007	0.033	0.933	0.904	0.896
1390	immed.	0.005	0.027	-0.009	0.022	0.388	0.364	0.365
1330	~5min	0.005	0.026	-0.009	0.020	0.359	0.335	0.336
8520	immed.	0.018	0.050	-0.009	0.031	1.030	0.990	0.988
8550	~5min	0.018	0.055	-0.009	0.032	1.120	1.074	1.073
1390	immed.	0.000	0.033	-0.012	0.022	0.481	0.450	0.455
1350	~5min	-0.001	0.032	-0.012	0.022	0.452	0.420	0.426
ULTIMATE FAILURE DATA								
9130				cks increasing i				
9650	Hold 2 min	Crack heard 1:	17 into loa	d, both end bea			at mortar (lo	wer) locations
		Panel Failure						
				e occurred appr				
11020	Horizontal s	al shear failure approximately 31 inches from left bearing end (concrete and mortar breaks)						
	Wall not fully	/ separated fron	n wire mes	h and foam core	e. Left end b	pearing morta	ar/foam crusł	ning 6.5" from er
	Right end be	earing mortar/for	am crushin	g approx 4" - 6"	from end.	-		
	Foam core a	at both end bear	ing location	ns began to squ	ish down fir	st, the morta	r breaks follo	owed

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 5670 lbs, Transducers 2 & 4 (RHS end) showing movement due to foam crushing

*At Load = 8050 lbs, One loud crack and pop heard, large crack formation on RHS end bearing mortar (lower).

Photos taken, no additional visible damage present

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1160.0	4640.0	0.000	0.0000	0.000
3560.0	14240.0	0.178	0.0148	0.066
4600.0	18400.0	0.298	0.0248	0.112
5670.0	22680.0	0.416	0.0346	0.146
6820.0	27280.0	0.589	0.0491	0.201
8050.0	32200.0	0.896	0.0747	0.336
8550.0	34200.0	1.073	0.0894	0.426

Stiffness (Flexural Rigidity) EI (lbs-ft ²)	1012421
Max Load (Ibs)	11020

Emmedue S.P.A

Intertek

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

2

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

Client: Project No: Product: Technician(s): Test Method(s):

M2 1504X8FRF3 Single Polystyrene PSM150 4' x 8' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
93	7.750	4.00	8.00	9.500	

Deflection Limit (L/x)	Load (Ibs-in)	1	5
L/ 120	7305.28		
L/ 180	5889.81		
L/ 240	5182.07		
L/ 360	4474.33		↓ FRONT

Linear Regression Analysis

5479.25608 3058.85694 566.735215 372.619861 0.95896269 443.123274 93.4722717 4 18354050.4 785432.944



Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 5479.26 + 3058.86

1/5/09 Page 50

11/28/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_1504X12FRF1 Single Polystyrene PSM150 4' x 12' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Wall Area (in^2): 48.00 1250

Project #: 3083303

g/m

Eng. Initials:

Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

56 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 47 inches apart

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
141	11.750	4.0	12.0	9.500	

Piston Load (lbs) Time Trans 1 (in.) Trans 2 (in.) Trans 3 (in.) Trans 5 (in.) Trans 5 (in.) Trans 6 (in.) Mdspan (in.) 1250 immed. 0.000 0.000 0.000 0.000 0.000 0.000 2520 immed. 0.002 0.000 0.014 0.003 0.270 0.283 0.281 2530 -5min 0.002 0.000 0.014 0.003 0.171 0.168 0.165 1510 -5min 0.002 0.001 0.015 0.004 0.503 0.491 0.491 3030 -5min 0.001 -0.002 0.233 0.004 0.538 0.524 0.524 1620 immed. 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3430 immed. 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 34450 -5min 0.000 -0.002 0.023 0.031 0.375 0.366			Out	Outer Corner Measurements Lateral Measurements				-		
1250 immed. 0.000 0.001 0.011 0.001 0.002 0.023 0.004 0.503 0.491 0.491 3030 -5min 0.000 -0.002 0.023 0.002 0.340 0.330 0.330 1530 immed. 0.000 -0.002 0.023 0.005 0.653 0.633 0.633 1530 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.612 3430 immed. 0.002 -0.023	Piston Load (lbs)	Time	Trans 1 (in)	Trans 2	Trans 3 (in)	Trans 4	Trans 5	Trans 6	Midspan	
2520 immed. 0.002 0.000 0.014 0.003 0.270 0.263 0.281 2530 -5min 0.002 0.000 0.014 0.003 0.171 0.168 0.165 1530 immed. 0.002 0.001 0.015 0.004 0.166 0.164 0.165 2990 immed. 0.000 -0.002 0.023 0.004 0.503 0.491 0.491 3030 -5min 0.000 -0.002 0.023 0.004 0.538 0.523 0.524 1620 immed. 0.000 -0.002 0.023 0.002 0.330 0.330 1530 -5min 0.000 -0.002 0.023 0.005 0.663 0.612 0.633 3450 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 -5min 0.002 -0.023 0.003 0.375 0.364 0.344 1600 immed.	Tiston Loud (163)	Time	fruits r (iii.)	(in.)	Trans & (iii.)	(in.)		(in.)		
2530 -5min 0.002 0.000 0.014 0.004 0.299 0.294 0.292 1530 immed. 0.002 0.000 0.014 0.003 0.171 0.166 0.164 1510 -5min 0.000 0.015 0.004 0.503 0.491 0.491 2990 immed. 0.000 -0.002 0.023 0.004 0.538 0.523 1620 immed. 0.000 -0.002 0.023 0.002 0.340 0.330 0.331 1530 -5min 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3450 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.347 4010 immed. 0.002 -0.003 0.300 0.007 0.830 0.811 0.812 4020 -5min		immed.				0.000				
1530 immed. 0.002 0.000 0.014 0.003 0.171 0.168 0.165 1510 -5min 0.002 0.001 0.015 0.004 0.166 0.164 0.160 2990 immed. 0.000 -0.002 0.023 0.004 0.533 0.491 3030 -5min 0.001 -0.002 0.023 0.004 0.533 0.523 1620 immed. 0.000 -0.002 0.023 0.002 0.340 0.330 0.330 1530 -5min 0.000 -0.002 0.023 0.005 0.653 0.637 0.638 3430 immed. 0.000 -0.002 0.023 0.003 0.375 0.366 0.384 1520 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.384 1520 -5min 0.002 -0.023 0.004 0.460 0.447 0.446 1530 -5min 0.002		immed.	0.002	0.000	0.014	0.003	0.270	0.263	0.261	
1510 5min 0.002 0.001 0.015 0.004 0.166 0.164 0.160 2990 immed. 0.000 -0.002 0.023 0.004 0.503 0.491 0.491 3030 -5min 0.001 -0.002 0.023 0.004 0.538 0.523 1620 immed. 0.000 -0.002 0.023 0.002 0.340 0.330 0.330 1530 -5min 0.000 -0.002 0.023 0.005 0.652 0.610 0.612 3430 immed. 0.000 -0.002 0.023 0.005 0.653 0.637 0.638 1600 immed. 0.002 -0.023 0.003 0.375 0.366 0.364 1520 -5min 0.000 -0.002 0.023 0.003 0.375 0.368 0.344 4010 immed. 0.002 -0.038 0.007 0.880 0.841 0.843 4020 -5min 0.002 <td>2530</td> <td>~5min</td> <td>0.002</td> <td>0.000</td> <td>0.014</td> <td>0.004</td> <td>0.299</td> <td>0.294</td> <td>0.292</td> <td></td>	2530	~5min	0.002	0.000	0.014	0.004	0.299	0.294	0.292	
2990 immed. 0.000 -0.002 0.023 0.004 0.503 0.491 0.491 3030 -5min 0.001 -0.002 0.023 0.004 0.538 0.523 0.524 1620 immed. 0.000 -0.002 0.023 0.002 0.340 0.330 0.330 1530 -5min 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3450 -5min 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3450 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.384 1600 immed. 0.002 -0.023 0.003 0.358 0.344 0.347 4010 immed. 0.002 -0.003 0.030 0.007 0.880 0.842 0.422 5170 immed. 0.002 0.028 0.004 0.460 0.444 0.422 5170 immed. <td></td> <td>immed.</td> <td></td> <td>0.000</td> <td>0.014</td> <td>0.003</td> <td></td> <td></td> <td></td> <td></td>		immed.		0.000	0.014	0.003				
3030 5min 0.001 -0.002 0.023 0.004 0.538 0.523 0.524 1620 immed. 0.000 -0.002 0.023 0.002 0.340 0.330 0.330 1530 -5min 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3430 immed. 0.000 -0.002 0.023 0.005 0.653 0.637 0.638 1600 immed. 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 -5min 0.000 -0.002 0.023 0.007 0.830 0.811 0.812 4010 immed. 0.002 -0.003 0.300 0.007 0.860 0.842 0.843 1600 immed. 0.000 -0.002 0.028 0.004 0.460 0.447 0.446 1530 -5min 0.000 -0.002 0.032 0.011 1.227 1.200 1.284	1510	~5min	0.002	0.001	0.015	0.004	0.166	0.164	0.160	
1620 immed. 0.000 -0.002 0.023 0.002 0.340 0.330 0.330 1530 -5min 0.000 -0.002 0.023 0.002 0.321 0.311 0.311 3430 immed. 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3450 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 -5min 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1600 immed. 0.002 -0.023 0.003 0.375 0.366 0.364 1600 immed. 0.002 -0.003 0.030 0.007 0.830 0.811 0.812 1600 immed. 0.002 -0.028 0.004 0.460 0.444 0.422 5170 immed. 0.010 -0.002 0.032 0.011 1.227 1.200 1.201 5170 -5min </td <td>2990</td> <td>immed.</td> <td>0.000</td> <td>-0.002</td> <td>0.023</td> <td>0.004</td> <td>0.503</td> <td>0.491</td> <td>0.491</td> <td></td>	2990	immed.	0.000	-0.002	0.023	0.004	0.503	0.491	0.491	
1530 5min 0.000 -0.002 0.023 0.002 0.321 0.311 0.311 3430 immed. 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3450 -5min 0.000 -0.002 0.023 0.005 0.653 0.637 0.638 1600 immed. 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 -5min 0.000 -0.002 0.023 0.003 0.358 0.348 0.347 4010 immed. 0.002 -0.003 0.300 0.007 0.860 0.842 0.843 1600 immed. 0.002 -0.028 0.004 0.460 0.447 0.446 1530 -5min 0.000 -0.002 0.029 0.041 1.227 1.200 1.201 5170 immed. 0.010 -0.002 0.053 0.047 0.595 0.615 0.578 5510 </td <td>3030</td> <td>~5min</td> <td>0.001</td> <td>-0.002</td> <td>0.023</td> <td>0.004</td> <td>0.538</td> <td>0.523</td> <td>0.524</td> <td></td>	3030	~5min	0.001	-0.002	0.023	0.004	0.538	0.523	0.524	
3430 immed. 0.000 -0.002 0.023 0.005 0.626 0.610 0.612 3450 -5min 0.000 -0.002 0.023 0.005 0.653 0.637 0.638 1600 immed. 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 -5min 0.000 -0.002 0.023 0.003 0.358 0.348 0.347 4010 immed. 0.002 -0.003 0.030 0.007 0.880 0.842 0.843 1600 immed. 0.000 -0.002 0.028 0.004 0.460 0.447 0.446 1530 -5min 0.001 -0.002 0.032 0.011 1.227 1.200 1.201 5170 immed. 0.009 -0.002 0.053 0.048 0.635 0.615 0.578 5510 immed. 0.002 0.053 0.047 0.595 0.615 0.578 5510 <td>1620</td> <td>immed.</td> <td>0.000</td> <td>-0.002</td> <td>0.023</td> <td>0.002</td> <td>0.340</td> <td>0.330</td> <td>0.330</td> <td></td>	1620	immed.	0.000	-0.002	0.023	0.002	0.340	0.330	0.330	
3450 -5min 0.000 -0.002 0.023 0.005 0.653 0.637 0.638 1600 immed. 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 -5min 0.002 -0.023 0.003 0.358 0.348 0.347 4010 immed. 0.002 -0.003 0.030 0.007 0.830 0.811 0.812 4020 -5min 0.002 -0.003 0.030 0.007 0.860 0.842 0.843 1600 immed. 0.000 -0.002 0.028 0.004 0.460 0.447 0.446 1530 -5min 0.001 -0.002 0.032 0.011 1.227 1.200 1.201 5170 immed. 0.009 -0.002 0.056 0.054 1.307 1.320 1.284 1630 immed. 0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. <td>1530</td> <td>~5min</td> <td>0.000</td> <td>-0.002</td> <td>0.023</td> <td>0.002</td> <td>0.321</td> <td>0.311</td> <td>0.311</td> <td></td>	1530	~5min	0.000	-0.002	0.023	0.002	0.321	0.311	0.311	
1600 immed. 0.000 -0.002 0.023 0.003 0.375 0.366 0.364 1520 ~5min 0.000 -0.002 0.023 0.003 0.358 0.348 0.347 4010 immed. 0.002 -0.003 0.030 0.007 0.830 0.811 0.812 4020 ~5min 0.002 -0.003 0.030 0.007 0.880 0.842 0.843 1600 immed. 0.000 -0.002 0.029 0.004 0.460 0.447 0.446 1530 ~5min 0.000 -0.002 0.029 0.004 0.436 0.424 0.422 5170 immed. 0.010 -0.002 0.053 0.048 0.635 0.655 0.618 1540 ~5min 0.008 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.062 -0.001 0.130 0.061 1.535 1.560 1.484 <	3430	immed.	0.000	-0.002	0.023	0.005	0.626	0.610	0.612	
1520 -5min 0.000 -0.002 0.023 0.003 0.358 0.348 0.347 4010 immed. 0.002 -0.003 0.030 0.007 0.830 0.811 0.812 4020 -5min 0.002 -0.003 0.030 0.007 0.860 0.842 0.843 1600 immed. 0.000 -0.002 0.028 0.004 0.460 0.447 0.446 1530 -5min 0.000 -0.002 0.029 0.004 0.436 0.424 0.422 5170 immed. 0.010 -0.002 0.032 0.011 1.227 1.200 1.284 1630 immed. 0.009 -0.002 0.055 0.615 0.578 1540 -5min 0.008 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.080 0.058 1.441 1.463 1.412 5510 -5min <td>3450</td> <td>~5min</td> <td>0.000</td> <td>-0.002</td> <td>0.023</td> <td>0.005</td> <td>0.653</td> <td>0.637</td> <td>0.638</td> <td></td>	3450	~5min	0.000	-0.002	0.023	0.005	0.653	0.637	0.638	
4010 immed. 0.002 -0.003 0.030 0.007 0.830 0.811 0.812 4020 ~5min 0.002 -0.003 0.030 0.007 0.860 0.842 0.843 1600 immed. 0.000 -0.002 0.028 0.004 0.460 0.447 0.446 1530 ~5min 0.000 -0.002 0.029 0.004 0.436 0.424 0.422 5170 immed. 0.010 -0.002 0.032 0.011 1.227 1.200 1.201 5170 ~5min 0.013 -0.002 0.056 0.054 1.307 1.320 1.284 1630 immed. 0.009 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.080 0.58 1.441 1.463 1.412 5510 ~5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 <t< td=""><td>1600</td><td>immed.</td><td>0.000</td><td>-0.002</td><td>0.023</td><td>0.003</td><td>0.375</td><td>0.366</td><td>0.364</td><td></td></t<>	1600	immed.	0.000	-0.002	0.023	0.003	0.375	0.366	0.364	
4020 -5min 0.002 -0.003 0.030 0.007 0.860 0.842 0.843 1600 immed. 0.000 -0.002 0.028 0.004 0.460 0.447 0.446 1530 -5min 0.000 -0.002 0.029 0.004 0.436 0.424 0.422 5170 immed. 0.010 -0.002 0.032 0.011 1.227 1.200 1.201 5170 -5min 0.013 -0.002 0.056 0.054 1.307 1.320 1.284 1630 immed. 0.009 -0.002 0.053 0.047 0.595 0.615 0.578 1540 -5min 0.008 -0.021 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.080 0.58 1.441 1.463 1.412 1530 -5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 <tr< td=""><td>1520</td><td>~5min</td><td>0.000</td><td>-0.002</td><td>0.023</td><td>0.003</td><td>0.358</td><td>0.348</td><td>0.347</td><td></td></tr<>	1520	~5min	0.000	-0.002	0.023	0.003	0.358	0.348	0.347	
1600 immed. 0.000 -0.002 0.028 0.004 0.460 0.447 0.446 1530 ~5min 0.000 -0.002 0.029 0.004 0.436 0.424 0.422 5170 immed. 0.010 -0.002 0.032 0.011 1.227 1.200 1.201 5170 ~5min 0.013 -0.002 0.056 0.054 1.307 1.320 1.284 1630 immed. 0.009 -0.002 0.053 0.047 0.595 0.615 0.578 1540 ~5min 0.008 -0.002 0.058 1.441 1.463 1.412 5510 immed. 0.023 -0.001 0.130 0.061 1.535 1.560 1.484 1660 immed. 0.062 -0.001 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA ULTIMATE FAILURE DATA 6010 Hold 2 min Wall deflecting more, pops and cracks heard	4010	immed.	0.002	-0.003	0.030	0.007	0.830	0.811	0.812	
1530 ~5min 0.000 -0.002 0.029 0.004 0.436 0.424 0.422 5170 immed. 0.010 -0.002 0.032 0.011 1.227 1.200 1.201 5170 ~5min 0.013 -0.002 0.056 0.054 1.307 1.320 1.284 1630 immed. 0.009 -0.002 0.053 0.048 0.635 0.655 0.618 1540 ~5min 0.008 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.058 1.441 1.463 1.412 5510 -5min 0.064 -0.001 0.125 0.054 0.772 0.804 0.728 1660 immed. 0.062 -0.001 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA ULTIMATE FAILURE DATA 6010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage </td <td>4020</td> <td>~5min</td> <td>0.002</td> <td>-0.003</td> <td>0.030</td> <td>0.007</td> <td>0.860</td> <td>0.842</td> <td>0.843</td> <td></td>	4020	~5min	0.002	-0.003	0.030	0.007	0.860	0.842	0.843	
5170 immed. 0.010 -0.002 0.032 0.011 1.227 1.200 1.201 5170 5min 0.013 -0.002 0.056 0.054 1.307 1.320 1.284 1630 immed. 0.009 -0.002 0.053 0.048 0.635 0.655 0.618 1540 -5min 0.008 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.080 0.058 1.441 1.463 1.412 5510 -5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 1660 immed. 0.062 -0.001 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA ULTIMATE FAILURE DATA ULTIMATE FAILURE DATA 0.6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) locatic 6010 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (1600	immed.	0.000	-0.002	0.028	0.004	0.460	0.447	0.446	
5170 ~5min 0.013 -0.002 0.056 0.054 1.307 1.320 1.284 1630 immed. 0.009 -0.002 0.053 0.048 0.635 0.655 0.618 1540 ~5min 0.008 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.080 0.058 1.441 1.463 1.412 5510 ~5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 1660 immed. 0.062 -0.001 0.122 0.053 0.720 0.751 0.677 1530 ~5min 0.060 0.000 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA ULTIMATE FAILURE DATA ULTIMATE FAILURE DATA 0.0401 0.122 0.053 0.720 0.751 0.677 0.010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage 6610	1530	~5min	0.000	-0.002	0.029	0.004	0.436	0.424	0.422	
1630 immed. 0.009 -0.002 0.053 0.048 0.635 0.655 0.618 1540 ~5min 0.008 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.080 0.058 1.441 1.463 1.412 5510 ~5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 1660 immed. 0.062 -0.001 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA ULTIMATE FAILURE DATA 0.6610 0.677 0.677 0.677 ULTIMATE FAILURE DATA Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) locatic 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) locatic 7160 Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right beari	5170	immed.	0.010	-0.002	0.032	0.011	1.227	1.200	1.201	
1540 ~5min 0.008 -0.002 0.053 0.047 0.595 0.615 0.578 5510 immed. 0.023 -0.002 0.080 0.058 1.441 1.463 1.412 5510 -5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 1660 immed. 0.062 -0.001 0.125 0.054 0.772 0.804 0.728 1530 ~5min 0.060 0.000 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA Other Allure Data Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) location Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire mers Left end bearing mortar/foam crushing approximately 6" - 9" from end. -9" from end. <td>5170</td> <td>~5min</td> <td>0.013</td> <td>-0.002</td> <td>0.056</td> <td>0.054</td> <td>1.307</td> <td>1.320</td> <td>1.284</td> <td></td>	5170	~5min	0.013	-0.002	0.056	0.054	1.307	1.320	1.284	
5510 immed. 0.023 -0.002 0.080 0.058 1.441 1.463 1.412 5510 ~5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 1660 immed. 0.062 -0.001 0.125 0.054 0.772 0.804 0.728 1530 ~5min 0.060 0.000 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA 6010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) locatic Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire mer Left end bearing mortar/foam crushing approximately 6" - 9" from end.	1630	immed.	0.009	-0.002	0.053	0.048	0.635	0.655	0.618	
5510 ~5min 0.064 -0.001 0.130 0.061 1.535 1.560 1.484 1660 immed. 0.062 -0.001 0.125 0.054 0.772 0.804 0.728 1530 ~5min 0.060 0.000 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA 6010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) location Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire measure Left end bearing mortar/foam crushing approximately 6" - 9" from end.	1540	~5min	0.008	-0.002	0.053	0.047	0.595	0.615	0.578	
1660 immed. 0.062 -0.001 0.125 0.054 0.772 0.804 0.728 1530 ~5min 0.060 0.000 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA 6010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) location Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire measure Left end bearing mortar/foam crushing approximately 6" - 9" from end.	5510	immed.	0.023	-0.002	0.080	0.058	1.441	1.463	1.412	
1530 ~5min 0.060 0.000 0.122 0.053 0.720 0.751 0.677 ULTIMATE FAILURE DATA 6010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) location Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire mest Left end bearing mortar/foam crushing approximately 6" - 9" from end.	5510	~5min	0.064	-0.001	0.130	0.061	1.535	1.560	1.484	
ULTIMATE FAILURE DATA 6010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) location Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load 7160 Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire mean the second	1660	immed.	0.062	-0.001	0.125	0.054	0.772	0.804	0.728	
6010 Hold 2 min Wall deflecting more, pops and cracks heard, no additional visible damage 6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) location Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire measured the dearing mortar/foam crushing approximately 6" - 9" from end.	1530	~5min	0.060	0.000	0.122	0.053	0.720	0.751	0.677	
6610 Hold 2 min Cracks heard 32 seconds into load, both end bearings beginning to crack at mortar (lower) location Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load 7160 Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire measured to bearing mortar/foam crushing approximately 6" - 9" from end.										
Panel Failure Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load 7160 Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire mean Left end bearing mortar/foam crushing approximately 6" - 9" from end.	6010	Hold 2 min	Wall deflecting	more, pop	s and cracks he	ard, no ado	ditional visible	e damage		
 Wall no longer able to hold load. Failure occurred approx 24 seconds into holding load Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire mean Left end bearing mortar/foam crushing approximately 6" - 9" from end. 	6610	Hold 2 min	Cracks heard 3	32 seconds	s into load, both	end bearing	gs beginning	to crack at r	nortar (lower)	locations
7160 Complete horizontal shear failure approximately 66.5 inches from right bearing end (concrete, mortar, wire mes Left end bearing mortar/foam crushing approximately 6" - 9" from end.										
Left end bearing mortar/foam crushing approximately 6" - 9" from end.		Wall no long	nger able to hold load. Failure occurred approx 24 seconds into holding load							
Left end bearing mortar/foam crushing approximately 6" - 9" from end.	7160	Complete ho								
No additional crusing at right end bearing		No additiona	I crusing at righ	t end bear	ing					
Foam core at left end bearing location began to squish down first, then the mortar breaks followed			0 0		•	down first,	then the mo	rtar breaks f	ollowed	

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 3030 lbs, several pops heard while taking wall to this load, no visible damage present

*At Load = 4020 lbs, one pop heard, no visible damage

*At Load = 5170 lbs, Transducers 3 & 4 showed significant movement after two pops heard approx 2:10 into load Wall inspected, no visible damage

*At Load = 5510 lbs, crushing of concrete, mortar, and foam core at Transducer 3 and 4 location. Photos taken At Transducer 3 location, foam squishing and mortar beginning to crack. At Transducer 4 location, concrete crack formation 16" from end of wall, foam showing evidence of squishing.

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1250.0	5000.0	0.000	0.0000	0.000
2530.0	10120.0	0.292	0.0243	0.160
3030.0	12120.0	0.524	0.0437	0.311
3450.0	13800.0	0.638	0.0532	0.347
4020.0	16080.0	0.843	0.0702	0.422
5170.0	20680.0	1.284	0.1070	0.578
5510.0	22040.0	1.484	0.1237	0.677

Stiffness (Flexural Rigidity) EI (lbs-ft ²)	1200867
Max Load (lbs)	7160

Emmedue S.P.A

Intertek

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

Client: Project No: Product: Technician(s): Test Method(s):

M2_1504X12FRF1 Single Polystyrene PSM150 4' x 12' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio

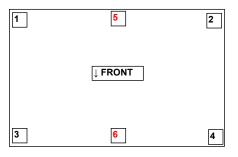
ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
141	11.750	4.00	12.00	9.500	

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	4805.42
L/ 180	3795.04
L/ 240	3289.84
L/ 360	2784.65

Linear Regression Analysis

2579.69936 1774.27142 85.7795611 80.8309641 0.99559675 88.0304702 904.420823 4 7008685.88 30997.4547



Equation of Best Fit Line

Load (lbs-in) = Defl. (in) x 2579.70 +

1774.27

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11/28/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_1504X12FRF2 Single Polystyrene PSM150 4' x 12' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05

Project #: 3083303

g/m

Eng. Initials:

Wall Area (in^2):48.00Pre-Load (lbs)1190Age of Wall:56 datLoad Method:Third-Bearing Type:1 inch

56 days (at test date) Third-Point Loading

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 47 inches apart

Support Span		Panel			
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)	
141	11.750	4.0	12.0	9.500	

		Out	er Corner	Measurements		Lateral Mea	surements	
Piston Load (lbs)	Time	Trans 1 (in.)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan
	Time		(in.)	Trans 5 (m.)	(in.)	(in.)	(in.)	Mean (in.)
1190	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2530	immed.	0.003	0.006	0.006	0.030	0.259	0.256	0.247
2550	~5min	0.004	0.010	0.006	0.031	0.283	0.278	0.268
1480	immed.	0.003	0.009	0.006	0.026	0.158	0.152	0.143
1430	~5min	0.003	0.009	0.006	0.026	0.149	0.143	0.135
3150	immed.	0.007	0.014	0.008	0.034	0.426	0.416	0.406
3170	~5min	0.006	0.016	0.008	0.034	0.460	0.448	0.438
1520	immed.	0.004	0.015	0.007	0.029	0.252	0.240	0.232
1440	~5min	0.003	0.014	0.006	0.028	0.235	0.222	0.216
3640	immed.	0.009	0.020	0.010	0.038	0.609	0.596	0.583
3650	~5min	0.010	0.020	0.010	0.038	0.655	0.644	0.630
1570	immed.	0.006	0.017	0.007	0.030	0.365	0.353	0.344
1460	~5min	0.005	0.017	0.006	0.030	0.338	0.326	0.318
4020	immed.	0.012	0.023	0.008	0.039	0.827	0.805	0.796
4030	~5min	0.013	0.023	0.009	0.040	0.883	0.863	0.852
1570	immed.	0.009	0.018	0.005	0.032	0.498	0.481	0.473
1460	~5min	0.008	0.018	0.004	0.032	0.464	0.448	0.441
5100	immed.	0.015	0.104	0.004	0.056	1.264	1.200	1.187
5110	~5min	0.015	0.170	0.004	0.081	1.395	1.302	1.281
1590	immed.	0.015	0.150	-0.001	0.072	0.757	0.679	0.659
1480	~5min	0.015	0.147	0.000	0.070	0.711	0.636	0.616
5420	immed.	0.021	0.216	0.002	0.098	1.550	1.438	1.410
5430	~5min	0.021	0.262	0.002	0.115	1.644	1.516	1.480
1610	immed.	0.021	0.255	-0.002	0.122	0.915	0.800	0.759
1500	~5min	0.021	0.250	-0.001	0.119	0.866	0.753	0.712
			ULTI	MATE FAILURE	E DATA			
6250	Hold 2 min	Transducer 2 I	ocation cru	shing, popping	and crackin	g heard. Cra	ck formation	at that location
0		extending the	entire pane	l width (all the w	ay to Trans	sducer 4 loca	tion)	
		Panel Failure						
	Wall no long	er able to hold load. Failure occurred approx 8 seconds into holding load						
6680		prizontal shear failure approximately 80 inches from right bearing end (concrete, mortar, wire mesh						
		aring mortar/foam crushing approximately 9" from end.						
	0	0		ring concrete/foa				
		•		n began to squis		t, then the m	ortar breaks	followed

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen

*All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 2550 lbs, one loud pop heard, Transducer 4 picking up movement, no visible damage or slippage

*At Load = 3170 lbs, Transducers 2 and 4 showing movement, no visible damage

*At Load = 4030 lbs, cracking and popping heard approx 1:05 into load, no visible damage

*At Load = 5110 lbs, crushing of foam core at Transducer 2 location. Photos taken

At same location, mortar beginning to crack underneath wall, approx 16" - 18" away from right bearing end

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under

third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1190.0	4760.0	0.000	0.0000	0.000
2550.0	10200.0	0.268	0.0223	0.135
3170.0	12680.0	0.438	0.0365	0.216
3650.0	14600.0	0.630	0.0525	0.318
4030.0	16120.0	0.852	0.0710	0.441
5110.0	20440.0	1.281	0.1068	0.616
5430.0	21720.0	1.480	0.1233	0.712

Stiffness (Flexural Rigidity) EI (lbs-ft ²)	1085571
Max Load (Ibs)	6680

Intertek

Client: Emmedue S.P.A Project No: M2_1504X12FRF2 Product: Technician(s): V. Burgos, Intertek San Antonio Test Method(s):

Single Polystyrene PSM150 4' x 12' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar)

ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

1

3

Sup	port Span		Panel	
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)
141	11.750	4.00	12.00	9.500

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	4804.35
L/ 180	3893.75
L/ 240	3438.44
L/ 360	2983.14

Linear Regression Analysis

2324.94972 2072.53647 105.767216 98.6255104 0.99178978 112.728762 483.197843 4

6140368.9 50831.0953

Equation of Best Fit Line Load (lbs-in) = Defl. (in) x 2324.95

2072.54

+

Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

5

FRONT

6

2

4

11/29/2007

Emmedue S.P.A

Test: Date: Client: Product ID: Product: Eng/Tech(s): Test Method(s):

M2_1504X12FRF3 Single Polystyrene PSM150 4' x 12' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) V. Burgos, Intertek San Antonio ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05

Project #: 3083303

ø/m

Eng. Initials:

Wall Area (in^2): Pre-Load (lbs) Age of Wall: Load Method: Bearing Type:

1520 57 days (at test date) Third-Point Loading

48.00

0

1 inch diameter steel rollers resting on 3 inch wide steel bearing plates (1/4" thick), located on all four points For third-point loading, bearings were spaced out 47 inches apart

Support Span		Panel				
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)		
141	11.750	4.0	12.0	9.500		

		Out	er Corner	Measurements	i	Lateral Mea	surements	
Piston Load (lbs)	Time	Trans 1 (in.)	Trans 2	Trans 3 (in.)	Trans 4	Trans 5	Trans 6	Midspan
	Time	, , , , , , , , , , , , , , , , , , ,	(in.)		(in.)	(in.)	(in.)	Mean (in.)
1520	immed.	0.000	0.000	0.000	0.000	0.000	0.000	0.000
2590	immed.	0.001	-0.001	0.002	0.020	0.140	0.155	0.142
2610	~5min	0.001	-0.001	0.005	0.022	0.156	0.175	0.159
1580	immed.	0.001	-0.002	0.005	0.014	0.029	0.035	0.028
1530	~5min	0.001	-0.002	0.005	0.014	0.018	0.022	0.016
3550	immed.	-0.001	-0.006	0.017	0.047	0.469	0.519	0.480
3570	~5min	-0.003	-0.006	0.019	0.048	0.571	0.615	0.578
1630	immed.	-0.002	-0.006	0.019	0.034	0.272	0.300	0.274
1560	~5min	-0.002	-0.006	0.019	0.034	0.250	0.276	0.251
3740	immed.	-0.002	-0.006	0.020	0.056	0.613	0.663	0.621
3750	~5min	-0.002	-0.005	0.022	0.057	0.638	0.689	0.646
1660	immed.	-0.001	-0.006	0.022	0.039	0.308	0.343	0.312
1560	~5min	-0.001	-0.006	0.021	0.038	0.276	0.309	0.279
4350	immed.	-0.002	-0.006	0.024	0.064	0.802	0.864	0.813
4380	~5min	0.000	-0.003	0.026	0.068	0.871	0.940	0.883
1690	immed.	0.000	-0.005	0.026	0.047	0.418	0.462	0.423
1550	~5min	0.001	-0.005	0.026	0.047	0.372	0.413	0.375
5210	immed.	-0.003	0.001	0.029	0.092	1.230	1.317	1.244
5210	~5min	-0.005	0.002	0.031	0.096	1.366	1.458	1.382
1690	immed.	-0.002	-0.002	0.029	0.070	0.707	0.774	0.717
1570	~5min	0.000	-0.002	0.029	0.067	0.648	0.714	0.658
5690	immed.	-0.008	0.004	0.034	0.105	1.700	1.800	1.716
5690	~5min	-0.010	0.004	0.039	0.105	1.856	1.969	1.878
1650	immed.	-0.005	-0.001	0.038	0.077	1.002	1.080	1.014
1560	~5min	-0.004	-0.002	0.038	0.077	0.955	1.029	0.965
			ULTI	MATE FAILURE	DATA			
6130	Hold 2 min	Popping heard	while takir	ng wall to this loa	ad. No addi	tional visible	damage pre	sent
		I			el Failure	-		
6470	Complete ho No end bear	prizontal shear fait	ailure appr sent on eith	e occurred while oximately 76 inc ner side				
	No additiona	al visible damag	е					

1/5/09 Page 56

Additional Notes: *The loads reported are the piston force only and DO NOT take account the weight of each wall specimen *All floor/roof walls were tested with the concrete side up (compression side)

*At Load = 3570 lbs, 4 to 5 pops heard during the first 10 seconds into load. Additional popping at 3 minutes No visible damage present

*At Load = 4380 lbs, pop heard 1 minute into load, mortar crack found (under wall) approx 59.5" from left end *At Load = 5210 lbs, cracking and popping heard. Concrete crack found between concrete and foam approx 15" long from right end (at Transducer 4 location). Foam break approx 3" down at right end of wall. At same location, Transducer 4 showing movement.

*Positive numbers indicate transducers extending outward; Negative numbers indicate transducers extending inward *The wall stiffness (EI) was calculated from the maximum deflection equation of a simply supported beam under third-point loading conditions

Load (lbs)	Load (lbs-ft)	Load Defl. (in)	Load Defl. (ft)	Set Defl. (in)
1520.0	6080.0	0.000	0.0000	0.000
2610.0	10440.0	0.159	0.0132	0.016
3570.0	14280.0	0.578	0.0482	0.251
3750.0	15000.0	0.646	0.0538	0.279
4380.0	17520.0	0.883	0.0736	0.375
5210.0	20840.0	1.382	0.1151	0.658
5690.0	22760.0	1.878	0.1565	0.965

Stiffness (Flexural Rigidity) El (lbs-ft^2)	664263
Max Load (lbs)	6470

Intertek

Client: Emmedue S.P.A M2_1504X12FRF3 Project No: Product: Single Polystyrene PSM150 4' x 12' x 9.5" Floor/Roof Flexural Wall Panel (Nominal 2.5" of concrete, 1.0" of mortar) Technician(s): V. Burgos, Intertek San Antonio Test Method(s):

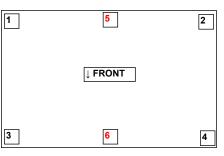
ICC-AC 15 - Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems Section 4.2.2.6 Floor or Roof Panel Flexural Tests in accordance with the general guidelines of ASTM E 72-05 Load achieved within 1 minute

Sup	oport Span		Panel	
(in)	(ft)	Width (ft)	Length (ft)	Thickness (in)
141	11.750	4.00	12.00	9.500

Deflection Limit (L/x)	Load (Ibs-in)
L/ 120	4660.54
L/ 180	3953.52
L/ 240	3600.00
L/ 360	3246.49

Linear Regression Analysis

1805.17227 2539.46404 161.289564 174.09427 0.96905547 222.512672 125.263565 4 6202035.78 198047.558



Note: Transducers 1 through 4 measured the outer deflections. Transducers 5 through 6 measured the lateral deflections.

Transducer 1: Upper left Transducer 2: Upper right Transducer 3: Lower left Transducer 4: Lower right Transducer 5: Midspan top Transducer 6: Midspan bottom

Equation of Best Fit Line Load (lbs-in) = Defl. (in) x 1805.17

2539.46

+

APPENDIX C Test Photographs

Note: Only a small number of photos were selected for this report. A CD copy of all the project photos will be provided to the client





80_4X8FRF3 (Setup and Failure Modes)

Figure 1A: Rear view of wall



Figure 2A: Transverse-flexural transducer locations





Figure 3A: 80_4X8FRF3 Failure mode



Figure 4A: 80_4X8FRF3 Failure mode (close-up)





150_4X12FRF3 (Setup and Failure Modes)

Figure 5A: 150_4X12FRF3 Setup



Figures 6A: Lateral transducer setup





Figure 7A: 150_4X12FRF3 Failure mode



Figure 8A: Failure mode (close-up)





PRE-TEST INSPECTION REPORT

Inspection Date:	July 1-2, 2007	Intertek Inspector:	Matt Lansdowne, EIT
Inspector's Tel:	(604) 520 - 3321	Inspector's Email:	matt.lansdowne@intertek.com
Product Name:	Emmedue Structurally Insulated Pane	els	

Project #: 3083303 Production Lot #: 07/01-02/07 # of Samples: See back page

General Instruction(s): Please complete ALL sections of this report. When information is not applicable, indicate "NA" and provide an explanation. Installation Instructions and MSDS sheets are required. Attach to this form, other product information, which is critical for followup inspections and ongoing certification. Please use the enclosed page for manufacturer's shipment.

	Owner/Distributor	Manufacturer (If Different From Owner/Distributor)
Company Name:	Emmedue S.P.A.	SAME AS OWNER
Address:	Via Toniolo 39/b Z.I. Bellocchi 61032 Fano (PU) Italy	
Tel:	(0039) 0721 855650 / 1	Fax:
Email:	(0039) 0721 854030	
Contact Person:	Omero Bassotti	

FORMULATION (attach material specification sheet(s) or "Certificate of Analysis")

Material	Approved Supplier(s)	Specification	% Content
EPS	ISOPAK Adratica Spa	15AE (It. Gov. Standard)	No Grind
EPS	Sulpol		
Steel Coil	MEttallurgica Ledrense	2.4mm diam., 3.00mm diam., 2.50mm diam.	3.0mm Yield 793 N/mm2 2.5mm Yield 712N/mm2
Adhesive	DA.FO.TEC	ABATECK D40/R	Use to join under length EPS panels

MANUFACTURING PROCESS (attach flowchart and/or details)

EPS and Steel Coil received, COA inspected to ensure quality, moved into inventory. Hotwires are set to Dimension using automated system, operator checks manually to ensure. EPS cut to size. Metal wire is Checked COA and diam. (calibrated caliper), monthly yield, ultimate, and elongation checked with calibrated tensile equipment. Steel wire loaded in to automated system. Unrolled and straightened, passed through welder that joins vertical and horizontal steel columns in preset grid pattern. Steel grid and EPS block taken To automated joiner. The EPS has steel grid laid on bottom surface and top surface. Joiner welds two grid Surfaces together. Inspector verifies welds are present. If > 3% welds missing, manual welding done.

PRODUCT DESCRIPTION: See Next Page

OTHER COMMENTS

Emmedue buys completed component parts. Uses proprietary automated equipment to cut and weld

Components together forming completed EPS Steel Grid System. This system is taken onsite, where Customers follow Emmedue installation instructions to apply shot crete exterior facings.

> Intertek Testing Services NA Ltd. 1500 Brigantine Drive, Coquitlam, B.C., Canada, V3K 7C1 Phone: 604-520-3321 Fax: 604-524-9186



Intertek Testing Services NA Ltd. Inspector: Matt Lansdowne, EIT Email: matt.lansdowne@intertek.com

Phone: (604) 520-3321 ext. 112

EMMEDUE TEST SAMPLE SIZES July 1-2, 2007

Type of test Normative		Type of panel	Lengths	Height	Final thickness	Quantity of tests
Load Bearing Wall	ASMT E 119	PSM 80	10'	10'	6"	2
Floor/Roof Fire Test	ASMT E 119	PSM 80	10'	10'	6"	2
Mall Commencien	AC15 4.2.2.2	PSM 80	4'	8'	6"	5
Wall Compression	ASTM E 72	PSM 80	4'	14'	6"	5
Wall Flexural	AC15 4.2.2.3	PSM 80	4'	8'	6"	5
vyall i lexular	ASTM E 72	PSM 80	4'	14'	6"	4
Wall Flexural-	AC15 4.2.2.4	PSM 80	4'	8'	6"	5
Compression	ASTM E 72	PSM 80	4'	14'	6"	5
Wall Shear	AC15 4.2.2.5	PSM 80	8'	8'	6"	5
wan Sugar	ASTM E 72	PSM 80	8'	14'	6"	4
		PSM 80	4'	8'	7"	5
Floor/Roof Flexural	AC15 4.2.2.6	PSM 80	4'	12'	7"	6
	ASTM E 455	PSM 150	4'	8'	9.5"	6
		PSM 150	4'	12'	9.5"	6
Floor/Roof Diaphragm	AC15 4.2.2.7	PSM 80	4'	8'	6"	5
	ASTM E 455	PSM 80	4'	12'	6"	5
				To	tal panel	75





ALAMD CONCRETE PROENCYS, Ltd

Mix design report

Mix design No. :	2125044			C	ERTIF	ICATE NO
Plant :	3135371	Client :				
Compressive Strength :	Alamo Concrete Products, Ltd.	Project :				
Nominal size :	3 500 psi at 28 Day	w/c Ratio ;		0.55	aling and a second s	
Usage :	# \$ (3/8")	Slump ;		4.00 ± 1.0	00 in	
Placement :		Slump with S	SuperP ;			
		Air :		0.0 to 0.0	%	-
Mat	Constitu erial - Type - Supplier - City	lents				
17 Y 18 18 18 19 19 19 19 19 19 19 19 19 19 19 19 19	Stone & ;	Gon J	F.M. Sp. Gr.	Abs. Qt	y SSD	Volume
3/8" Limestone - # 8 (3/8")	- Alamo Concrete Products, Ltd.	Sana	10,000			
·		1117	2.580		780 15	11.05 ft
Mig Sand ACP - 0.39 in - A	Mamo Concrete Products , San Antoni	0	2.610	2.50 1	079 Jb	6.62 ft ³
Silica Sand - 0.39 in - Alam	o Concrete Products, Ltd.		2.630		466 Ib	2.84 ft°
	Cement & A	dditive			ĺ	
Portland - Type I/II LA - Al	amo Cement, San Antonio		3.150		376 lb	1.91 ft ^a
					57010	1.91 ff.
510 - Fly Ash Class C B	oral, Deely		2.720		94 lb	0.55 ft ⁹
Stondard mater Guardant	Water					
Standard water - Standard w	ater - Not defined		1.000	2	258 Ib	4.13 ft ^a
Nir			·			0.00 ft ³
61A - WRDA 35 - ASTM	Admixture & Other C 494 'Type A (Winter) - W.R. Grace,	s constituants		·····		
60A - Daratard 17 - ASTM	C 494 Type D (Summer) - W.R. Grace,	Houston	1.000	1	28 oz	0.01 ft ^a
	e with spread (canning) - with Ora	x, nousion	1.000	9.	40 oz.	0.01 ft°
agaaraan 1. casaanaanaa . casaanaanaan .	· · · · · · · · · · · · · · · · · · ·	· <u> </u>	Total	40	53 16	27.10 £³
nit Weight :	149.6 lb/ft ³	Total miz	cost:			2110 12
enarks :						
repared by : Chris G. Slate,	Technical Services Director Ap	proved by :				
	(



Description	Model No.	Serial No.	Last Calibration Date	Calibration Due Date
Load Cell	41A	1100639	4/17/07	4/17/08
LVDT	JEC-AG	L9233000	3/1/07	3/1/08
LVDT	JEC-AG	L9233400	3/1/07	3/1/08
LVDT	JEC-AG	L9300600	3/1/07	3/1/08
LVDT	JEC-AG	L9300700	3/1/07	3/1/08
LVDT	JEC-AG	L9301000	3/1/07	3/1/08
LVDT	JEC-AG	L9301100	3/1/07	3/1/08
LVDT	JEC-AG	L9233500	3/1/07	3/1/08
DAQ Cart	N/A	99LE004	5/27/07	11/27/08
DAQ Cart Recalibration	N/A	99LE004	11/27/07 5/27/08	
Stopwatch	14-649-9	61809410	8/15/07	8/15/08
3000 psi pressure gauge	N/A	298967	5/18/07 5/18/08	

List of Calibrated Instrumentation Used for Testing



REFERENCES

- 1) Emmedue Advanced Building Systems Operator's Manual, Rev. 02 or 3/19/2004, pp. 2-7, 15-16.
- 2) Acceptance Criteria for Sandwich Panels, ICC AC 04, Effective July 1, 2007, Section 4.4.1, p. 5.
- 3) Acceptance Criteria for Concrete Floor, Roof and Wall Systems and Concrete Masonry Wall Systems, ICC AC 15, Effective July 1, 2007.



REVISION SUMMARY

DATE	SUMMARY
January 5, 2009	Section 3.2 (Sample and Assembly Description); galvanized steel
	wire mesh diameters changed to 0.099 inches (transverse) and
	0.121 inches (longitudinal)
February 20, 2008	Original Report Issue Date

